

Enhancement of Bandwidth in Microstrip Patch Antenna using EBG

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ABSTRACT

This paper presents the bandwidth and gain enhancement of microstrip patch antenna using EBG for X band (10 GHz) application. The surface waves must be suppressed to increase the bandwidth and gain by using EBG. By using EBG the stop band characteristics is created over certain frequency and that has been adapted to suppress the surface wave and to enhance the gain and bandwidth of the antenna at the resonating frequency. The main goal of using EBG structures in microstrip antenna is to achieve better gain and efficiency, lower side-lobes and back-lobes levels, and better isolations among array elements, by suppressing surface wave modes. The plot of return loss, gain and directivity with and without EBG are compared in this paper. By using patch antenna with EBG structure the operating bandwidth reaches 27% in the band of frequency 10.2-13GHz.

Index Terms

Bandwidth, Electromagnetic band gap, Gain, Microstrip patch antenna, directivity.

1. INTRODUCTION

With the advancement in the technologies the microstrip patch antennas comes out with best results for wireless devices because of its advantages like low profile, light weight, low cost and ease of fabrication. The size of patch should be around half a wavelength for the structure to work as good radiator[1]. To overcome with the disadvantages of microstrip patch antenna i.e. excitation of surface wave, narrow bandwidth and low gain various techniques have been used namely micromachining [2,3], DGS(Defected ground structure)[4], periodic structures called electromagnetic bandgap (EBG)[5-8]. These methods have eliminated the bandwidth problem for most applications. But limitations of gain and surface wave excitation still remain. That is why, in recent years there has been considerable effort in the EBG structure for antenna application to suppress the surface wave and overcome the limitations of the antenna. The surface waves are reduced because of electromagnetic band gap created due to EBG structures. Recently, there is a great interest in realizing the high efficiency patch antenna on high permittivity substrate, including the use of the latest micromachining technology [2].

In this paper, we propose a design based on concept of electromagnetic band gap (EBG) structures for enhancement of gain and bandwidth and compare the results with the edge feed microstrip patch antenna operating at 10 GHz resonating frequency for X band applications. The surface wave which are excited in the dielectric substrate are suppressed by placing square-lattice metal pads with grounding vias beneath

the patch, which not only improves the gain but also increase its frequency bandwidth. It has been shown in article [9] that, placing EBG cells in *E*-plane is sufficient for surface wave reduction and it is not required to have *H*-plane EBG cells. This EBG structures is used in microstrip array antennas between radiating array elements in *E*-plane to reduce mutual coupling between them by suppressing surface waves. But we are using EBG structures in both *E*-plane and *H*-plane over a single microstrip patch antenna. Our proposed antenna gives better performance compare to the conventional rectangular microstrip patch antenna. A substantial gain and bandwidth enhancement has been obtained. The design and simulation have been done by using Advanced Design System Simulator (ADS).

2. ANTENNA DESIGN AND STRUCTURE DESCRIPTION

2.1 Microstrip patch antenna without ebg

For the known frequency and substrate parameters (h , ϵ_r and f_o) the size of antenna is calculated using the transmission line model. The equations for designing the patch antenna using transmission line model are given as[1]:

a. Width of patch

$$w = \frac{1}{2f\sqrt{\mu_0\epsilon_0}\sqrt{\epsilon_r + 1}} \sqrt{2}$$

b. Effective dielectric constant

$$\epsilon_{\text{reff}} = \frac{\epsilon_r + 1}{2} + \frac{\epsilon_r - 1}{2} \left[1 + 12 \frac{h}{w} \right]^{-2}$$

c. The extended patch length due to fringing field

$$\frac{\Delta l}{h} = 0.412 \frac{(\epsilon_{\text{reff}} + 0.3) \left(\frac{w}{h} + 0.264 \right)}{(\epsilon_{\text{reff}} - 0.3) \left(\frac{w}{h} + 0.8 \right)}$$

d. The actual length

$$L = L_{\text{eff}} - 2\Delta l$$

e. Effective length due to resonance

$$L_{eff} = \frac{\lambda_0}{2} = \frac{v}{2f}$$

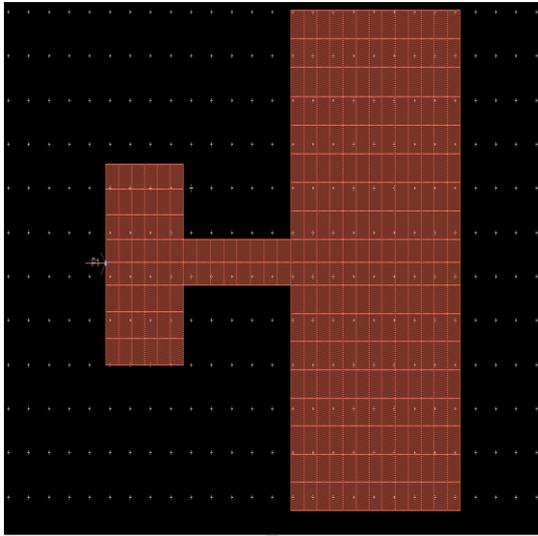


Fig 1. Microstrip patch without EBG structure in ADS tool

The patch antenna is fed through various feeding technique as microstrip line feeding, inset feeding, coaxial feeding, proximity coupling feeding and aperture couple feeding [1]. We are using microstrip line feed of 50 ohm impedance with the $\lambda/4$ transformer placed at the edge of patch on its width in this design. Fig 1 shows the proposed design of microstrip patch antenna on dielectric substrate having dielectric constant $\epsilon_r=2.5$ with height of substrate $h=1.5\text{mm}$, loss tangent=0.0022 and resonating frequency $f_0=10\text{ GHz}$. By using these substrate parameters the dimension of patch calculated as:

Length of patch $L=8.37\text{mm}$

Width of patch $w=11.338\text{mm}$

The width of the patch should be chosen larger than the length of patch in order to get the higher bandwidth. The antenna is designed to operate at 10 GHz frequency.

2.2 Microstrip patch antenna with ebg structures

Electromagnetic band gap structures are defined as artificial periodic objects that prevent/assist the propagation of electromagnetic waves in a specified band of frequency for all incident angles and all polarization states. Two commonly employed features are suppressing unwanted substrate modes and acting as an artificial magnetic ground plane. The main advantage of EBG structure is their ability to suppress the surface wave current. The generation of surface waves degrades the antenna efficiency and radiation pattern. Furthermore, it increases the mutual coupling of the antenna array which causes the blind angle of a scanning array EBG structures are periodic arrangement of dielectric materials and metallic conductors. They are categorized into three groups according to their geometric configuration: (a) three-dimensional volumetric structures, (b) two-dimensional planar surfaces, and (c) one-dimensional transmission lines[9]. In this proposed design we are using the 2-D mushroom type

EBG surfaces is shown in fig 3, which have the advantages of low profile, light weight, and low fabrication cost, and are widely considered in antenna engineering.

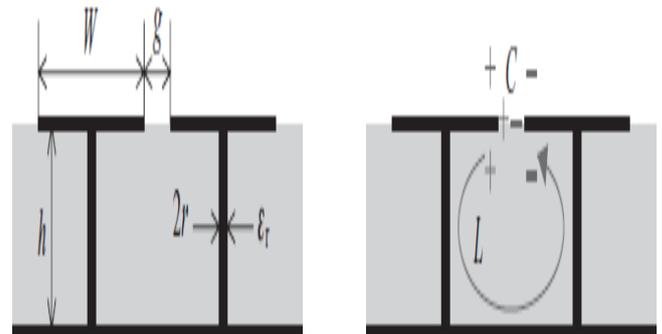
The parameters of the EBG structure are labeled in Fig. 2.a as patch width W , gap width g , substrate thickness h , dielectric constant ϵ_r , and vias radius r . When the periodicity $(W + g)$ is small compared to the operating wavelength, the operation mechanism of this EBG structure can be explained using an effective medium model with equivalent lumped LC elements, as shown in Fig.2b [10]. The capacitor results from the gap between the patches and the inductor results from the current along adjacent patches. The impedance of a parallel resonant LC circuit is given by:

$$Z = j\omega L / (1 - \omega^2 LC)$$

The resonance frequency of the circuit is calculated as following:

$$\omega_0 = 1/\sqrt{LC}$$

At low frequencies, the impedance is inductive and supports TM surface waves. It becomes capacitive at high frequencies and TE surface waves are supported. Near the resonance frequency ω_0 , high impedance is obtained and the EBG does not support any surface waves, resulting in a frequency band gap.



(a)

(b)

Fig 2. LC model for the mushroom-like EBG structure: (a) EBG parameters and (b) LC model[10]

The edge capacitance for the narrow gap situation is given by the following equation [10]:

$$C = \frac{W\epsilon_0(1+\epsilon_r)}{\pi} \cosh^{-1} \frac{(W+g)}{g}$$

The value of the inductor is derived from the current loop in Fig.2b, consisting of the vias and metal sheets. After a simple derivation, the inductance is expressed as below [10], which depends only on the thickness of the structure and the permeability:

$$L = \mu h$$

The microstrip patch drawn on EBG substrate is shown in fig 3. In this proposed design we taking the parameter of EBG structure as:

- a) The width of the metal pads $W= 5.5*5.5\text{ mm}$
- b) The gap width $g= 0.4\text{mm}$

c) The radius of via $r = 0.4\text{mm}$

and the other parameters like height of substrate and dielectric constant is taken same as in case of microstrip patch antenna without EBG.

The width varies from 0.04λ GHz to 0.20λ GHz, gap width varies from 0.01λ GHz to 0.12λ GHz and the substrate thickness, h varies from 0.01λ GHz to 0.09λ GHz. Here, λ means the wavelength respect to the GHz range frequency. These parameters are directly effecting the performance of EBG that why they are dependent on wavelength.

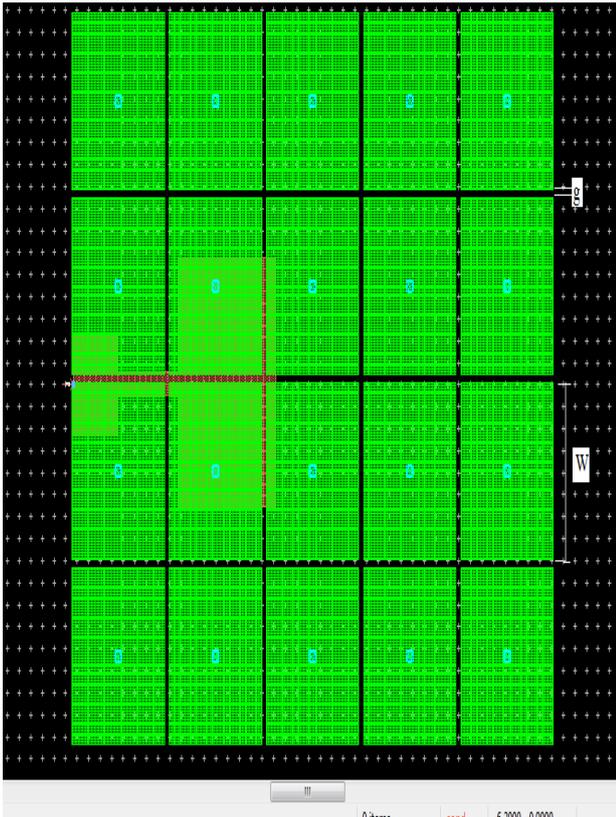


Fig 3.Microstrip patch antenna with 2D EBG structure on ADS

3. RESULTS AND DISCUSSION

It become easy to simulate the design through computer before real time implementation. The ADS tool helps us to determine the impedance bandwidth, return loss, gain and directivity. This simulator also helps to reduce the fabrication cost because only the antenna with the best performance would be fabricated. The simulated results of antenna with EBG and without EBG has been shown in fig 4 and fig 5.

3.1 Return loss and bandwidth

The return loss of patch antenna without EBG is -29.987db at 10 GHz resonating frequency and return loss of proposed antenna with EBG is -42.34db at 10.67 GHz resonating frequency. The negative value of return loss signifies that there are significantly less losses in the antenna.

The bandwidth can be calculated from fig 4 and fig 5. The bandwidth of patch antenna without EBG is from $9.75\text{--}10.25$

GHz i.e 4% and bandwidth of patch antenna with EBG is from $10.1\text{--}13\text{ GHz}$ which is 27.17% . The bandwidth of patch antenna with EBG is higher than the conventional patch antenna.

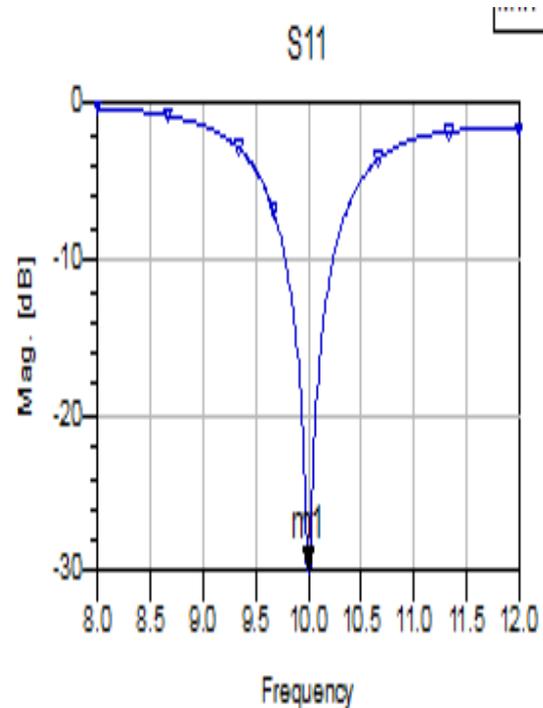


Fig 4.Return loss of microstrip patch antenna without EBG with $L=8.37\text{mm}$, $w=11.338\text{mm}$, $h=1.5\text{mm}$ and $\epsilon_r=2.5$.

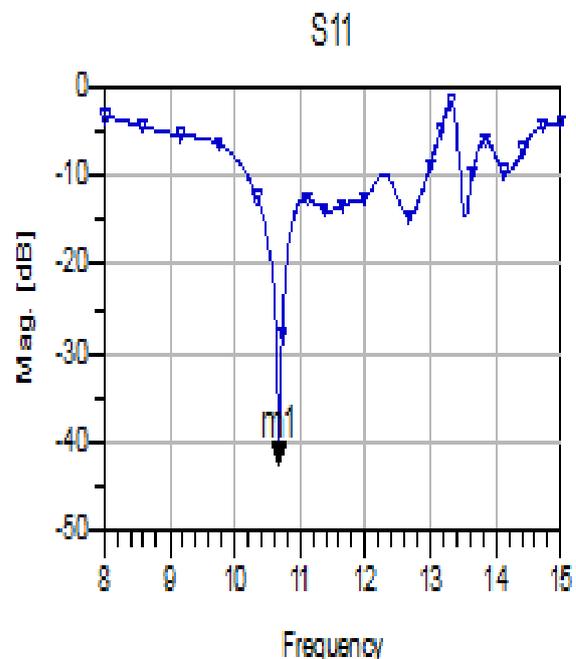


Fig 5.Return loss of microstrip patch antenna with EBG and with the same dimension as of conventional patch but width of metal pads $W=5.5\text{mm}$, gap width $g=0.4\text{mm}$ and radius of via $r=0.4\text{mm}$.

3.2 Gain and directivity

The antenna parameters of patch antenna without EBG and with EBG is shown in fig 6 and fig 7

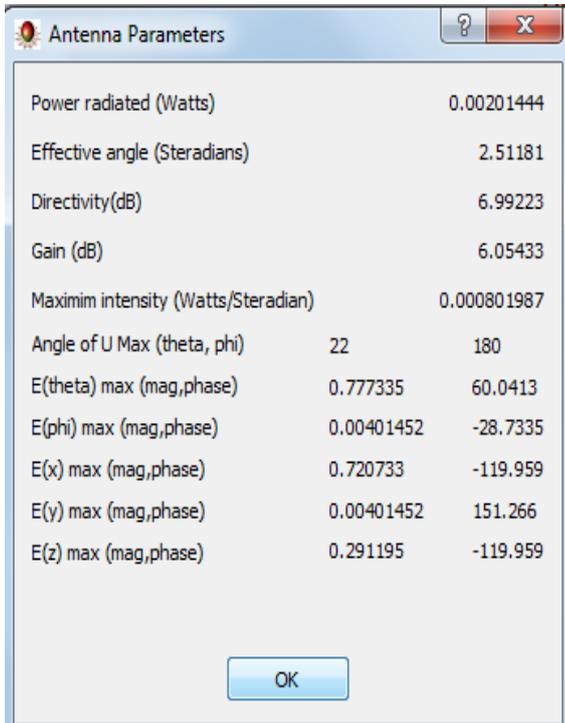


Fig 6. Antenna parameters of microstrip patch antenna without EBG

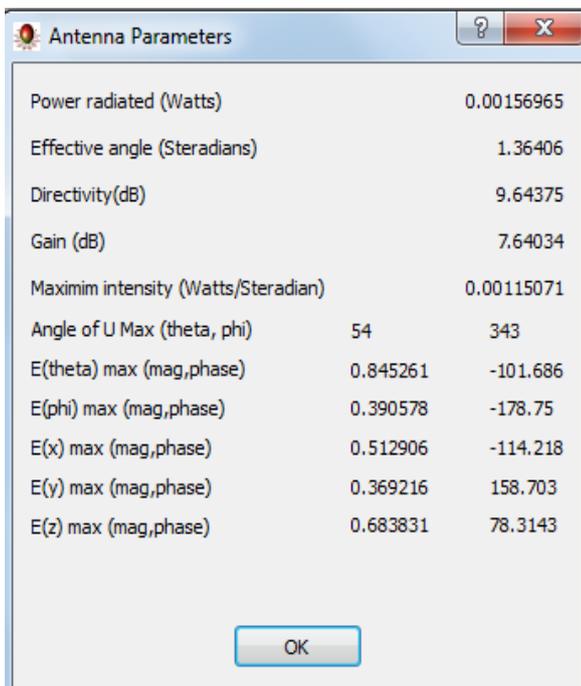


Fig 7. Antenna parameters of microstrip patch antenna with EBG

The gain of patch antenna without EBG is 6.05db and of antenna with EBG is 7.64db. The directivity of patch antenna without EBG is 6.99dbi and of antenna with EBG is 9.64dbi. The gain and directivity of microstrip patch antenna with EBG is greater than conventional patch antenna.

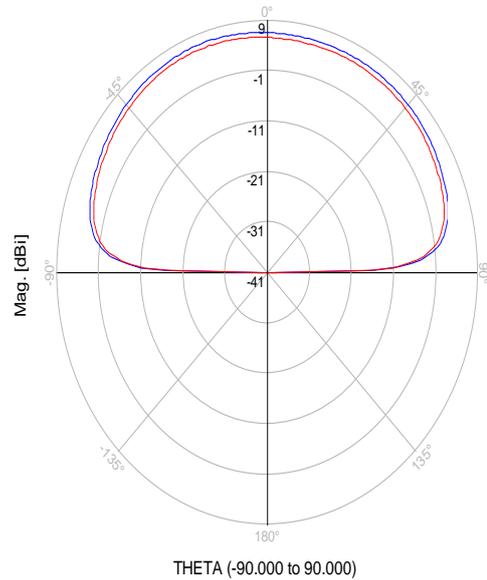


Fig 8. Gain and directivity of microstrip patch antenna without EBG

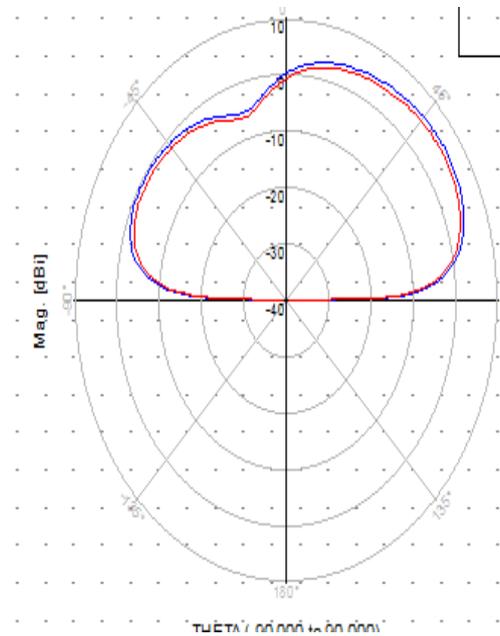


Fig.9. Gain and directivity of microstrip patch antenna with EBG

4. CONCLUSION

The purpose of this paper is to design microstrip patch antenna with EBG and without EBG with same dimension at 10 GHz frequency so that it can be used for X band application and compare the results. From the simulated results we can see that the performance of patch with EBG is better

than patch without EBG. The gain and bandwidth also improves when EBG is added on the patch.

5. REFERENCES

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