

Effect of Different Membership Functions on Fuzzy Power System Stabilizer for Synchronous Machine Connected to Infinite Bus

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1. ABSTRACT

The effectiveness of power system stabilizer (PSS) in providing damping and improving the dynamic response is well established. In this paper focuses, the performance of single machine infinite bus is studied with fuzzy power system stabilizer (FPSS). The generator is represented by the standard K-coefficients as second order system. The mechanism to discuss the rules is described and the performance is investigated for trapezoidal, triangular and Gaussian membership functions of input and output variables. For FPSS, speed deviation and acceleration deviation are taken as input. The system is simulated in SIMULINK environment and performance is investigated for transients due to change in input of varying magnitude.

Keywords

Power System Stabilizer, Synchronous Machine, Single Machine Infinite Bus System, Fuzzy Logic, Simulink

2. INTRODUCTION

The conventional power plants of 1950s were equipped with continuously acting automatic voltage regulators to improve the transient stability of system. The high gain of these voltage regulators has a destabilizing effect on power system. The power oscillations of small magnitude and high frequency, which often persisted in power system, present the limitation to the amount of power transmitted within the system. Improved performance has been achieved by adding damping to the system by employing power system stabilizers (PSS). The conventional PSS, which uses lead-lag compensation, is resulting into poor performance under different loading conditions [1]-[2] as the gain settings are designed for specific condition. In the early years, a stabilizer providing good performance under various operating conditions could not be designed. The fuzzy logic control has been suggested as a possible solution to this problem. Metwally and Malik [2] described fuzzy power system stabilizer using generator speed and output power variation as the controller input variables. Taliyat *et al.* [3] presented the design of augmented fuzzy power system stabilizer to enhance power system stability. Hiyama [4] derived acceleration, speed deviation and phase deviation of generator from measured real power signal. Majid *et al.* [5] presented a fuzzy controller in which speed deviation and rotor acceleration were taken as inputs. Juan *et al.* [6] compared the fuzzy and rule based power system stabilizers. Gupta *et al.* [7].

proposed a robust FPSS using speed deviation and rotor acceleration as inputs for multi machine system and studied the performance using different defuzzification methods.

Moodley *et al.* [8] investigated the effect of FLPSS in a multi-machine environment. Ferreira *et al.* [9] proposed a FPSS including a fuzzy PI controller to improve steady state behavior of a system. Lim [10] proposed a fuzzy logic control scheme using only one input signal which is derived as the linear combination of signal, signal derivative and signal integral.

In this paper, the performance of single machine infinite bus system with fuzzy power system stabilizer is presented. The generator is represented by second order system with the help of standard K-constant representation. The speed deviation and acceleration deviations are taken as the inputs. Performance is studied for trapezoidal, gaussian and triangular membership functions of fuzzy sets and compared with conventional lead-lag compensator. The simulation has been implemented in SIMULINK

3. SYSTEM MODELING

The system comprises of synchronous machine, excitation system and power system stabilizer model. The system model is developed as follows:-

3.1 Synchronous Machine Model

The configuration of synchronous machine connected to infinite bus through transmission network is represented as the Thevenin's equivalent shown in Fig. 1

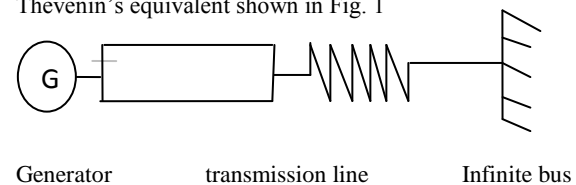


Fig.1: The equivalent of synchronous machine connected to infinite bus

The equations governing the machine model [11] are:-

$$S\Delta\omega_r = \frac{1}{2H} (T_m - T_e - K_D\Delta\omega_r) \quad (1)$$

$$S\Delta\delta = \omega_r \Delta\omega_r \quad (2)$$

Where,

$$\Delta Te = K_1 \Delta\delta + K_2 \Delta\psi_{fd} \quad (3)$$

$$\Delta\psi_{fd} = \frac{K_3}{1 + T_3 s} (\Delta E_{fd} - K_4 \Delta\delta) \quad (4)$$

Where, T_m and T_e are the prime mover input and electrical output torques respectively, H is the inertia constant, δ and ω are rotor angle and speed respectively

3.2 Excitation System Model

The thyristor excitation system as shown in Fig. 2 is considered. The nonlinearity associated with the ceilings EFMAX and EFMIN, is ignored for small-disturbance studies.

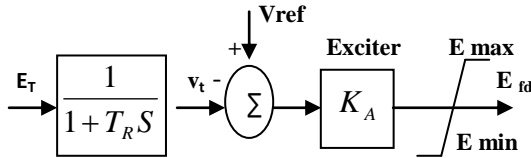


Fig. 2: Thyristor excitation system

The equations governing the exciter model are:-

$$s\Delta v_1 = \frac{1}{T_R} (\Delta E_t - \Delta v_1) \quad (5)$$

$$E_{fd} = k_A (V_{ref} - v_1) \quad (6)$$

$$\Delta E_t = K_5 \Delta\delta + K_6 \Delta\psi_{fd} \quad (7)$$

3.3 Power System Stabilizer Model

The PSS is used to provide damping to electromechanical oscillations. The PSS counters the oscillations by forcing the change in excitation level appropriately. Without PSS, the reduced damping in power system is due to phase lags resulted by the field time constants and the phase lags in the normal voltage regulation loop. The PSS uses phase compensation by adjusting the timing of correction signal opposing the rotor oscillations.

A power system stabilizer can Therefore increase the generator's damping coefficient. The PSS as shown in Fig. 3 has three components, the phase compensation block, the signal washout block and gain block. The phase compensation block provides the appropriate phase lead characteristics to compensate for the phase lag between exciter input and generator electrical torque. The signal washout block serves as high pass filter, with time constant T_w high enough to allow signals associated with oscillations in ω_r to pass

unchanged. The stabilizer gain KSTAB determines the amount of damping introduced by PSS. For the conventional PSS following transfer functions is considered.

$$\Delta v_2 = \frac{sT_w}{1 + sT_w} (K_{STAB} \Delta\omega_r) \quad (8)$$

$$\Delta v_s = \frac{1 + sT_1}{1 + sT_2} (\Delta v_2) \quad (9)$$

T_w is the washout filter time constant. The implementation of the PSS in K constant model is shown in Fig. 4.

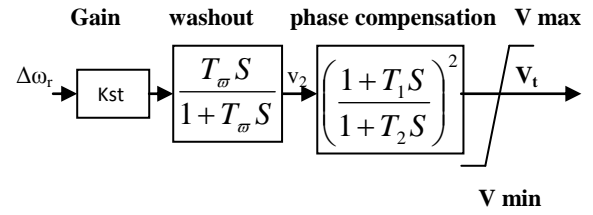


Fig. 3: Conventional lead-lag PSS

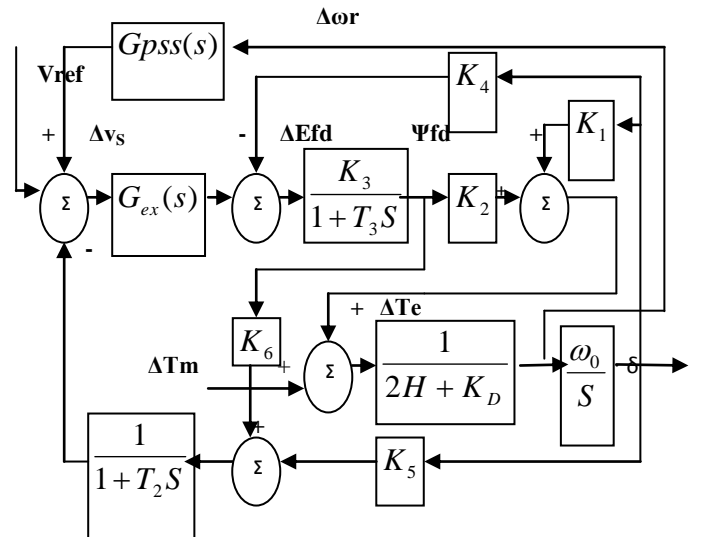


Fig. 4: Block diagram representation with AVR and PSS

4. FUZZY CONTROLLED POWER SYSTEM STABILIZER

4.1 Fuzzy Control System

Since the concept of fuzzy logic given by Zadeh in 1965, it has found applications in various areas including a controller for power system stabilizer [12]. A fuzzy controller, as shown in Fig. 5, comprises of four stages: fuzzification, a knowledge base, decision making and defuzzification. The fuzzification interface converts input data into suitable linguistic values that can be viewed as label fuzzy sets. The knowledge base comprises knowledge of application domain and attendant control goals by means of set of linguistic control rules. The decision making is the aggregation of output of various control rules that simulate the capability of human decision

making. The defuzzification inference performs scale mapping, which converts the range of values of output variables into corresponding universe of discourse

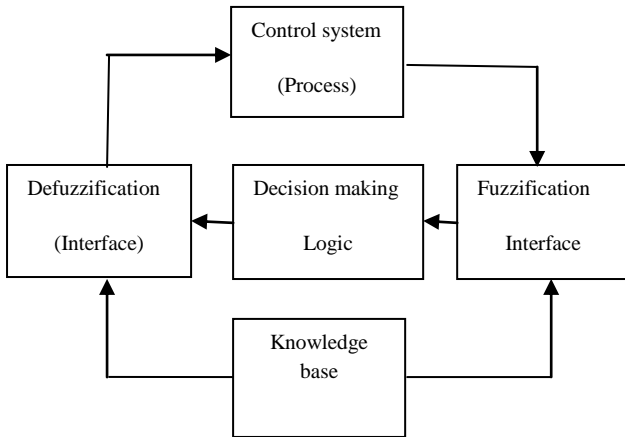


Fig. 5: The principle design of fuzzy logic controller

The fuzzy controller design consists of the following steps:-

- 1) Identification of input and output variables.
- 2) Construction of control rules.
- 3) Establishing the approach for describing system state in

terms of fuzzy sets, i.e. establishing fuzzification method and fuzzy membership functions. Selection of the compositional rule of inference. Defuzzification method transformation of the fuzzy control statement into specific control actions.

4.2 Generating Membership Functions

The method proposed by Hong *et al.* [13] which helps in generating membership functions has been used in FPSS. This method partitions a set of data into classes that can be used to derive membership functions. The method for obtaining membership function for a variable is explained as:-

Step1. Given a data set, there are n training samples. The values for the parameter x $\vec{X} = x_1, x_2 \dots x_n$,

are sorted into ascending order, denoted as

$$\vec{Y} = \text{Sort}[\vec{X}] = y_1, y_2 \dots y_n, \quad (11)$$

Step2. Calculate the difference between the adjacent data:

$$\text{diff}_i = y_{i+1} - y_i, \text{ for } i=(1,2,3,\dots,n-1),$$

Step3. The similarities between adjacent values are found and mapped into real numbers between 0 and 1 as:-

$$s_i = \left\{ \begin{array}{l} \left\{ 1 - \frac{\text{diff}_i}{C * \sigma_s} \text{ for } \text{diff}_i \leq C * \sigma_s \right\} \\ \left\{ 0 \text{ otherwise} \right\} \end{array} \right\} \quad (12)$$

Where,

σ_s is the standard deviation of diff_i and

C is the control parameter used to determine the shape of the membership function.

Step4. The data is grouped according to similarities. A

Threshold value α divides adjacent values into classes. If the similarity is greater than the threshold value, then the two adjacent values belong to the same class, otherwise the values are divided into different classes by creating a new class

$$\begin{array}{l} \text{if } (s_i \geq \alpha) \text{ then } y_i, y_{i+1} \in C_i \\ \text{Else } y_i \in C_i, y_{i+1} \in C_{i+1} \end{array} \quad (13)$$

where C_i and C_{i+1} denote two distinct classes for the same parameter.

Step5. The triangular membership function for each class is defined. For class j , it consists of three points: the central vertex point, b_j , and the two endpoints, a_j and c_j . The central vertex point is determined for each class and is calculated by the given formula:

$$b_j = \frac{y_i * s_i + y_{i+1} * \frac{s_i + s_{i+1}}{2} + \dots + y_{k-1} * \frac{s_{k-2} + s_{k-1}}{2} + y_k * s_{k-1}}{s_i + \frac{s_i + s_{i+1}}{2} + \dots + \frac{s_{k-2} + s_{k-1}}{2} + s_{k-1}}$$

Where, k represents the ending data index for this class, i.e., data y_i through y_k fall into class j , and s_i is the similarity between y_i and y_{i+1} . The endpoints a_j and c_j , are obtained using interpolation as:-

$$a_j = b_j - \frac{b_j - y_i}{1 - \mu_j(y_i)}, c_j = b_j + \frac{y_k - b_j}{1 - \mu_j(y_k)} \quad (14)$$

$\mu_j(y_i)$ and $\mu_j(y_k)$ is the membership expressed as:-

$$\mu_j(y_i) = \mu_j(y_k) = \min(s_i, s_{i+1}, \dots, s_{k-1})$$

4.3 Fuzzy Based PSS

The fuzzy power system stabilizer a two-input, a single-output component. The two inputs are change in angular speed and rate of change of angular speed whereas output of fuzzy logic controller is a voltage signal. The membership function of a variable is expressed into seven fuzzy sets defined in Table.1.

Table.1: Fuzzy sets of variable

NB	NEGATIVE BIG
NM	NEGATIVE MEDIUM
NS	NEGATIVE SMALL
ZE	ZERO
PS	POSITIVE SMALL
PM	POSITIVE MEDIUM
PB	POSITIVE BIG

The membership function maps the crisp values into fuzzy variables. The choice of membership functions has an important bearing on the performance of the fuzzy logic based PSS. A set of rules which define the relation between the inputs and output of fuzzy controller are defined using the linguistic variables. The knowledge required to generate the fuzzy rules can be derived from an offline simulation. However, it has been noticed that, for monotonic systems, a symmetrical rule table is very appropriate, although sometimes it may need slight adjustment based on the behavior of the specific system. If the system dynamics are not known or are highly nonlinear, trial-and-error procedures and experience play an important role in defining the rules. The two inputs, speed and acceleration, result in 49 rules for each machine as shown in Table.2. The typical rules are having the following structure

Rule 1: If speed deviation is NM (negative medium) AND acceleration is PS (positive small) then voltage (output of fuzzy PSS) is NS (negative small).

Rule 2: If speed deviation is NB (negative big) AND acceleration is NB (negative big) then voltage (output of fuzzy PSS) is NB (negative big).

Table.2: Rules for fuzzy PSS

Speed deviation	Acceleration						
	NB	NM	NS	ZE	PS	PM	PB
NB	NB	NB	NB	NB	NM	NM	NS
NM	NB	NM	NM	NM	NS	NS	ZE
NS	NM	NM	NS	NS	ZE	ZE	PS
ZE	NM	NS	NS	ZE	PS	PS	PM
PS	NS	ZE	ZE	PS	PS	PM	PM
PM	ZE	PS	PS	PM	PM	PM	PB
PB	PS	PM	PM	PB	PB	PB	PB

After replacing the conventional PSS block by fuzzy controller block, the representation of fuzzy logic controller implemented on single machine infinite bus system can be shown in the Fig. 6. The fuzzy module has two inputs namely the angular velocity and its derivative i.e. angular acceleration and output parameter as voltage. These are normalized by gains K_{in1} , K_{in2} and K_{out} respectively to match the range on which the membership functions are defined. Parameters K_{in1} , K_{in2} and K_{out} are tuned to give the desired response.

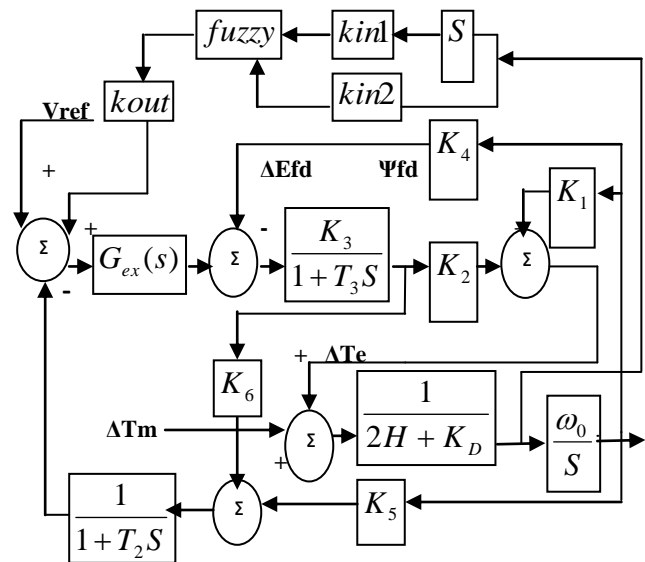


Fig. 6: Single machine infinite bus system with FPSS.

5. RESULTS AND DISCUSSION

The performance of single machine infinite bus system with lead-lag PSS and fuzzy PSS has been studied in SIMULINK environment. The fuzzy stabilizer has been Modeled in *fis* editor of matlab. The SIMULINK model of the system with fuzzy PSS is shown in Fig. 7. Corresponding to the system data specified in Appendix, the K-coefficients are calculated as $K_1=0.7636$, $K_2=0.8644$, $K_3=0.3231$, $K_4=1.4189$, $K_5 = -0.1463$, $K_6=0.4167$. The scaling factors associated with input and output variables are tuned and taken as $K_{in1}=1.8$, $K_{in2}=29.58$, $K_{out}=1.05$. For such constants, which are in Fig. 7, the performance has been studied under different conditions.

Although the stability problem in practical power system is mainly due to poor damping, the constant K_5 has important bearing on system performance. Its value normally found to be negative for high reactance and high power output, a practical situation. The K_5 can have positive value for low reactance and low power output. Therefore, the performance is studied for small 0.05 p.u. change in input for both K_5 negative (-0.1463) and K_5 positive (0.1463) and response characteristics are shown Fig. 8 and Fig. 9 respectively.

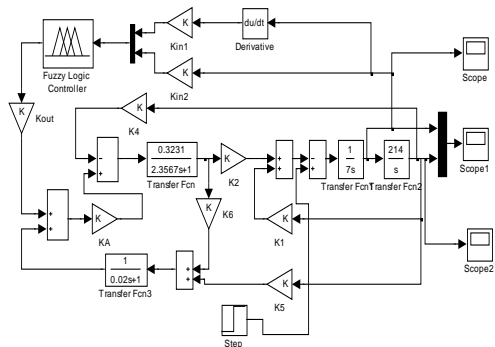


Fig. 7: SIMULINK model with fuzzy logic based PSS

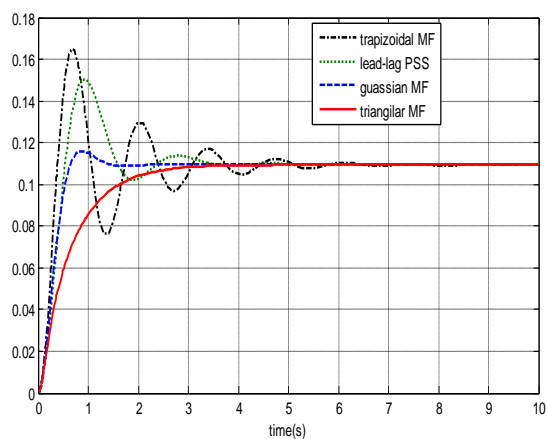


Fig. 8 (a): Angular position for a 0.05pu change in mechanical input with K5 positive

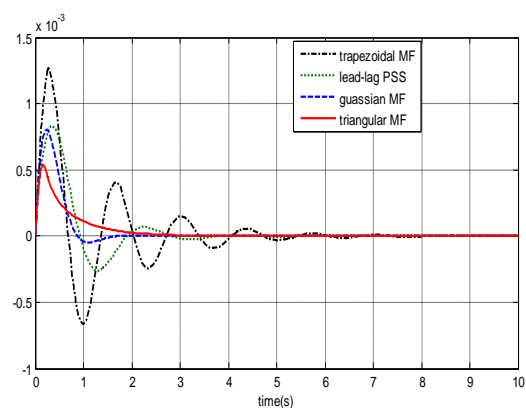


Fig. 8 (b): Angular speed for a 0.05pu change in mechanical input with K5 positive

As shown in Fig. 8(a) and Fig. 8(b), the oscillations are more pronounced in case of inputs and outputs having trapezoidal membership functions for K5 positive and the system become stable after a long time of 9 seconds approximately. With K5 negative, generally the practical case, the performance

characteristics are shown in Fig. 9(a) and Fig. 9(b). The unstable behavior is resulted if the trapezoidal membership function is used with negative value of K5. As evident from Fig. 8 and Fig. 9, the performance with trapezoidal membership functions is unsatisfactory and thus this membership function is not suited for the PSS design. The performance of lead-lag PSS and PSS using Gaussian and triangular membership functions is comparable and the system becomes stable after in nearly 3 seconds

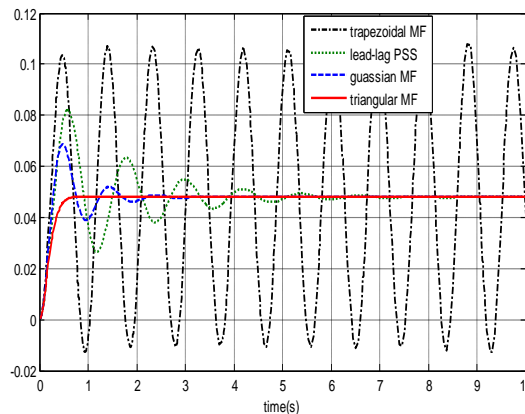


Fig. 9 (a): Angular position for a 0.05pu change in mechanical input with K5 negative.

With the Gaussian membership, the performance may be affected by the change in the spread of the membership function. The effect of change in the spread of Gaussian membership is therefore studied and the results are presented in Fig. 10 for negative value of K5. With the increase in the spread of Gaussian membership function, oscillations are reduced and system becomes stable after 3.5 seconds. However, the unstable response is resulted with decreased spread. The oscillations are reduced considerably in case the inputs and outputs having triangular membership functions and system become stable after 0.5 seconds approximately.

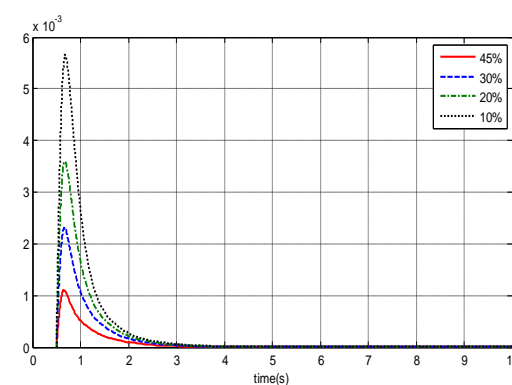


Fig. 9 (b): Angular speed for a 0.05pu change in mechanical input with K5 negative.

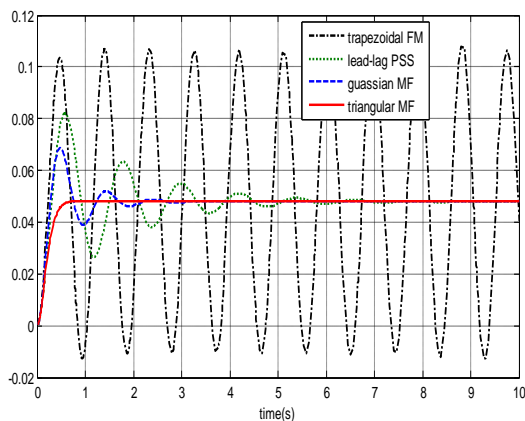


Fig. 10 (a): Angular position for a 0.05pu change in mechanical input with K5 negative with the change in spread of Gaussian membership function

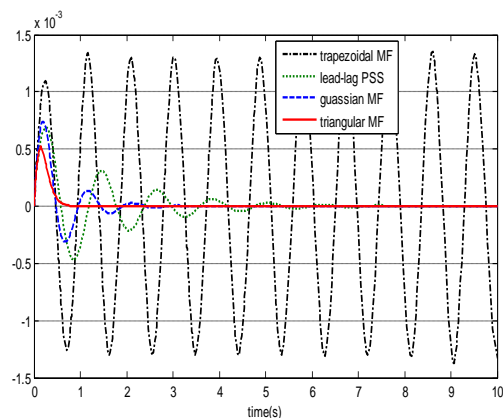


Fig. 10 (b): Angular position for a 0.05pu change in mechanical input with K5 negative with the change in spread of Gaussian membership function.

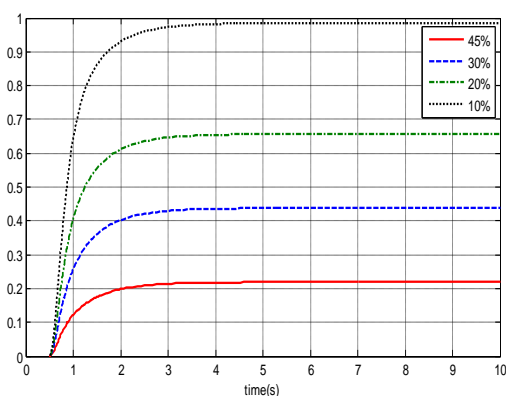


Fig. 11 (a): Angular position for different operating conditions using fuzzy PSS

The response for different operating conditions using triangular membership functions is investigated for negative value of K5 and the performance characteristics are shown in Fig. 11 for 10%, 20%, 30% and 45% change in mechanical input. With triangular membership functions, the response is

coming out to be stable in all the cases with very less oscillations thus enhancing the stability of a system. As seen in Fig. 8-11, the performance of FPSS with triangular membership function is superior in comparison to the performance with other PSS

6. CONCLUSION

The simulation studies support that the fuzzy PSS provide the better damping of oscillations as compared to conventional PSS (lead-lag). However, the choice of Member ship functions has an important bearing on the damping of oscillations. The oscillations are more pronounced in case of trapezoidal membership functions. The response with gauss membership functions having increased spread is comparable to triangular membership functions. However, the performance of FPSS with triangular membership functions is superior compared to other PSS.

7. APPENDIX

Synchronous machine parameters:

$P=0.9$, $Q=0.3$, $E_t=1.0$, $f=50$, $X_d=1.81$, $X_q=1.76$, $X_{d1}=0.3$, $X_L=0$, $X_e=0.65$, $R_a=0.003$, $T_{d01}=8.0$, $H=3.5$, $\omega=314$, $K_d=0$, $T_R=0.02$, $E_{Tmag}=1.0$, $L_{adu}=1.65$, $L_{adu}=1.60$, $R_{fd}=0.0006$, $L_{fd}=0.153$, $K_{sd}=0.849$, $K_{sq}=0.849$, $K_{sdI}=0.434$, $K_{sqI}=0.434$, $ASAT=0.031$, $BSAT=6.93$, $\Psi_1=0.8$,

Frequency of oscillation(in rad/sec)=10. The standard IEEE type ST1A excitation system model has been considered for the study with parameters as: - $K_A = 200$, $T_R = 0.02$. The parameters of PSS are:- $T_1=0.154$, $T_2=0.033$.

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