Hall Effects on Unsteady MHD Free Convective Flow Past an Accelerated Moving Vertical Plate with Viscous and Joule Dissipations

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ABSTRACT

Hall effects on an unsteady MHD free convective flow of a viscous incompressible electrically conducting fluid past a uniformly accelerated vertical plate in the presence of a uniform transverse applied magnetic field have been investigated on taking viscous and Joule dissipations into account. The governing partial differential equations have been solved numerically by applying a Crank - Nicolson's type of implicit finite difference method with a tri-diagonal matrix manipulation and an iterative procedure. The variations of the fluid velocity components and temperature distribution are presented graphically. It is found that the fluid velocity components are significantly affected by Hall parameter. An increase in Eckert number leads to rise in the fluid velocity components and temperature distribution. Further, it is found that the magnitude of the shear stress components at the plate increase with an increase in either Hall parameter or Eckert number or Prandtl number. The rate of heat transfer at the plate decreases with an increase in either Eckert number or Prandtl number or time.

Key words: Hall currents, MHD free convective flow, Prandtl number, Grashof number, Eckert number and viscous and Joule dissipations.

1. INTRODUCTION

Magnetohydrodynamics is currently undergoing a period of great enlargement and differentiation of subject matter. It is important in the design of MHD generators and accelerators in geophysics, underground water storage system, soil sciences, astrophysics, nuclear power reactor, solar structures and so on. The mechanism of conduction in ionized gases in the presence of strong magnetic field is different from that in metallic substance. The electric current in ionized gases is generally carried by electrons, which undergo successive collisions with other charged or neutral particles. In the ionized gases the current is not proportional to the applied potential except when the field is very weak in an ionized gas where the density is low and the magnetic field is very strong, the conductivity normal to the magnetic field is reduced due to the free spiraling of electrons and ions about the magnetic lines of force before suffering collisions and a current is induced in a direction normal to both electric and magnetic fields. This phenomenon is called the Hall effect. The study of Hall effects on MHD free convective flows has important engineering applications in problems of magnetohydrodynamic generators and Hall accelerators as well as in flight magnetohydrodynamics. It is also important in the solar physics involved in the sunspot development, the solar cycle and the structure of magnetic stars. The effect of Hall currents on hydromagnetic flow near a porous plate has been studied by Pop[1, 2]. Gupta [3] has examined the effect of Hall currents on the steady magnetohydrodynamic flow of an electrically conducting fluid

past infinite Oscillatory an porous flat plate. magnetohydrodynamic flow past a flat plate with Hall effects has been investigated by Datta and Jana [4]. The effect of Hall currents on hydromagnetic free convective flow near an accelerated porous plate has been studied by Hossain and Mohammad [5]. Pop and Watanabe [6] have described the Hall effects on magnetohydrodynamic free convection about a semiinfinite vertical flat plate. Effect of chemical and thermal diffusion with the Hall current on an unsteady hydromagnetic flow past an infinitely long vertical porous plate has been discussed by Acharya et al. [7]. Aboeldahab and Elbarbary [8] have analyzed the effect of Hall current on the magnetohydrodynamics free convective flow past a semiinfinite vertical plate with mass transfer. Takhar et al.[9] have investigated the unsteady free convective flow past an infinitely long vertical porous plate due to the combined effects of thermal and mass diffusion, magnetic field and Hall currents. Kinvaniui et al.[10] have studied the heat and mass transfer in unsteady free convective flow past an impulsively started infinite vertical porous plate with Hall current and radiation absorption. Hall effects on an MHD flow past a moving plate in a fluid have been studied by Takhar et al.[11]. Convective heat transfer from different geometries has received considerable attention in recent years owing to its importance in various technological applications such as fibre and granular insulation, electronic system cooling, cool combustors, oil extraction, thermal energy storage and flow through filtering devices. porous material regenerative heat exchangers. The book written by Bejan and Kraus [12] excellently describes the extent of the research information in this area. The viscous dissipation effects are important in geophysical flows and also in certain industrial operations and are usually characterized by the Eckert number. In the literature, extensive research work is available to examine the effect of natural convection on flow past a plate. Callahan and Manner [13] have first considered the transient free convective flow past a semi-infinite plate by explicit finite difference method. However, this analysis is not applicable for other fluids whose Prandtl number is different from unity. Soundalgekar and Ganesan [14] have analyzed transient free convective flow past a semi-infinite vertical flat plate, on taking into account mass transfer by an implicit finite difference method of Crank-Nicolson type. Das and Jana [15] have examined the heat and mass transfer effects on an unsteady MHD free convective flow past a moving vertical plate in a porous medium. In most of the studies mentioned above, viscous dissipation is neglected. Gebhart [16] has shown the importance of viscous dissipative heat in free convective flow in the case of isothermal and constant heat flux at the plate. Gebhart and Mollendorf [17] have considered the effects of viscous dissipation for external natural convective flow over a surface. Israel Cookey et al. [18] have investigated the influence of viscous dissipation and radiation on an unsteady MHD free convective flow past an infinitely long heated vertical plate in a

porous medium with time dependent suction. Srihari et al. [19] have studied an MHD free convective flow of an incompressible viscous dissipative fluid in an infinitely long vertical oscillating plate with constant heat flux. Suneetha et al. [20] have analyzed the effects of viscous dissipation and thermal radiation on hydromagnetic free convective flow past an impulsively started vertical plate. Babu et al. [21] have studied the radiation and chemical reaction effects on an unsteady MHD convective flow past a vertical moving porous plate embedded in a porous medium with viscous dissipation. Kishore et al. [22] have analyzed the effects of thermal radiation and viscous dissipation on MHD heat and mass diffusion flow past an oscillating vertical plate embedded in a porous medium with variable surface conditions. Hall effects on an unsteady MHD free convective flow past an impulsively started porous plate with viscous and Joule's dissipation have been studied by Anjali Devi et al. [23].

In the present paper, we have studied the Hall effects on an unsteady MHD free convective flow of a viscous incompressible electrically conducting fluid past an accelerated moving vertical plate on taking viscous and Joule dissipations into account. The governing equations have been solved numerically using Crank-Nicolson's method. It is found that the primary velocity u and the magnitude of the secondary velocity v increase with an increase in either Hall parameter m or Eckert number Ec or Grashof number Gr. It is also found that the fluid temperature θ increases with an increase in either Hall parameter m or Eckert number m or Eckert number Ec or Grashof number Gr or Grashof number Gr or Grashof number Fr. Further, it is found that the absolute values of the shear stresses τ_x and τ_y at the plate $\eta = 0$ increase with an increase in either m or Ec. The rate of heat transfor $\begin{pmatrix} \partial \theta \\ \partial \theta \end{pmatrix}$ of the plate m = 0 decreases with an

heat transfer $-\left(\frac{\partial\theta}{\partial\eta}\right)_{\eta=0}$ at the plate $\eta=0$ decreases with an

increase in either Eckert number Ec or Prandtl number Pr or time τ .

2. FORMULATION OF THE PROBLEM AND ITS SOLUTIONS

Consider the unsteady hydrodynamic flow of a viscous incompressible electrically conducting fluid past a uniformly accelerated vertical plate on taking viscous and Joule dissipations into account. Choose a Cartesian co-ordinates system such that the x-axis is taken along the vertical plate in an upward direction, z-axis is perpendicular to the plate and y-axis is taken normal to the zx-plane. At time $t \le 0$, both the fluid and the plate are at rest with constant temperature T_{∞} . At time t > 0, the plate at z = 0 starts to move in its own plane with a uniform velocity ct, c(>0) being a constant and T_w is the plate temperature. A uniform transverse magnetic field of strength H_0 is applied perpendicular to the plate [see Fig.1]. As the plate is infinitely long, the fluid velocity components and temperature distribution are functions of z and t only.



Figure 1. Geometry of the problem

The initial and boundary conditions of the problem are u' = v' = 0, $T = T_{\infty}$ at $t \le 0$ for all z,

$$u' = ct, v' = 0, T = T_w$$
 at $z = 0$ for all $t > 0$, (1)

 $u' \rightarrow 0, v' \rightarrow 0, T = T_{\infty} \text{ as } z \rightarrow \infty \text{ for all } t > 0,$

where u' and v' are the fluid velocity components in the x and y-directions respectively and T the fluid temperature.

The generalized Ohm's law, on taking Hall currents into account and neglecting ion-slip and thermo-electric effect, is (see Cowling [24])

$$\vec{J} + \frac{\omega_e \tau_e}{H_0} \left(\vec{J} \times \vec{H} \right) = \sigma \left(\vec{E} + \mu_e \vec{q} \times \vec{H} \right), \tag{2}$$

where \vec{J} is the current density vector, \vec{H} the magnetic field vector, \vec{E} the electric field vector, ω_e the cyclotron frequency, τ_e the electron collision time, σ the electrical conductivity of the fluid, μ_e the magnetic permeability and \vec{q} the fluid velocity vector.

We shall assume that the magnetic Reynolds number for the flow is small so that the induced magnetic field can be neglected. This assumption is justified since the magnetic Reynolds number is generally very small for partially ionized gases. The solenoidal relation $\nabla \cdot \vec{H} = 0$ for the magnetic field gives $H_z = H_0 =$ constant everywhere in the fluid where $\vec{H} \equiv (0,0,H_z)$. Further, if (J_x,J_y,J_z) be the components of the current density \vec{J} , then the equation of the conservation of the charge $\nabla \cdot \vec{J} = 0$ gives $J_{\vec{J}} = \text{constant}$. This constant is zero since $J_{z} = 0$ at the plate which is electrically non-conducting. Thus $J_{z} = 0$ everywhere in the flow. Since the induced field is neglected, magnetic Maxwell's equation $\nabla \times \vec{E} = -\mu_e \frac{\partial \vec{H}}{\partial t}$ becomes $\nabla \times \vec{E} = \vec{0}$ which gives $\frac{\partial E_x}{\partial z} = 0$

and $\frac{\partial E_y}{\partial z} = 0$. This implies that $E_x = \text{constant}$ and $E_y = \text{constant everywhere in the flow.}$

In view of the above assumption, the equation (2) gives

$$J_x + mJ_y = \sigma(E_x + \mu_e v'H_0), \tag{3}$$

$$J_{y} - mJ_{x} = \sigma(E_{y} - \mu_{e}u'H_{0}), \qquad (4)$$

where $m = \omega_e \tau_e$ is the Hall parameter.

At infinity, the magnetic field is uniform so that there is no current and hence, we have

$$J_x \to 0, J_y \to 0 \text{ as } z \to \infty.$$
 (5)

On the use of (1) and (5), equations (3) and (4) yield

$$E_x = 0, \quad E_y = 0 \tag{6}$$

everywhere in the flow.

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Substituting the values of E_x and E_y given by (6) in equations (3) and (4) and solving for J_x and J_y , we get

$$J_{x} = \frac{\sigma \mu_{e} H_{0}}{1 + m^{2}} (v' + mu'),$$
(7)
$$J_{y} = -\frac{\sigma \mu_{e} H_{0}}{1 + m^{2}} (u' - mv').$$
(8)

On the use of (7) and (8) and on using the usual Boussinesq approximation, the Navier-Stokes equations and energy equation can be written as

$$\frac{\partial u'}{\partial t} = v \frac{\partial^2 u'}{\partial z^2} + g \beta (T - T_{\infty}) - \frac{\sigma \mu_e^2 H_0^2}{\rho (1 + m^2)} (u' - mv'), \quad (9)$$

$$\frac{\partial v'}{\partial t} = v \frac{\partial^2 v'}{\partial z^2} - \frac{\sigma \mu_e^2 H_0^2}{\rho \left(1 + m^2\right)} (v' + mu'), \tag{10}$$

$$\rho c_{p} \frac{\partial T}{\partial t} = k \frac{\partial^{2} T}{\partial z^{2}} + \mu \left[\left(\frac{\partial u'}{\partial z} \right)^{2} + \left(\frac{\partial v'}{\partial z} \right)^{2} \right] + \sigma \mu_{e}^{2} H_{0}^{2} \left(u'^{2} + v'^{2} \right), \qquad (11)$$

where g is the acceleration due to gravity, β the coefficient of thermal expansion, μ the coefficient of viscosity, ν the kinematic viscosity, ρ the fluid density, k the thermal conductivity and c_p the specific heat at constant pressure.

Introducing the non-dimensional variables

$$u = \frac{u'}{(vc)^{\frac{1}{3}}}, v = \frac{v'}{(vc)^{\frac{1}{3}}}, \eta = z \left(\frac{c}{v^2}\right)^{\frac{1}{3}},$$
$$\tau = t \left(\frac{c^2}{v}\right)^{\frac{1}{3}}, \theta = \frac{T - T_{\infty}}{T_w - T_{\infty}},$$
(12)

equations (9), (10) and (11) become

$$\frac{\partial u}{\partial \tau} = \frac{\partial^2 u}{\partial \eta^2} + Gr\theta - \frac{M^2}{(1+m^2)}(u-mv), \tag{13}$$

$$\frac{\partial v}{\partial \tau} = \frac{\partial^2 v}{\partial \eta^2} - \frac{M^2}{(1+m^2)} (v + mu), \tag{14}$$

$$Pr\frac{\partial\theta}{\partial\tau} = \frac{\partial^{2}\theta}{\partial\eta^{2}} + PrEc\left[\left\{\left(\frac{\partial u}{\partial\eta}\right)^{2} + \left(\frac{\partial v}{\partial\eta}\right)^{2}\right\} + M^{2}\left(u^{2} + v^{2}\right)\right]$$
(15)

where $M^2 = \frac{\sigma \mu_e^2 H_0^2}{\rho} \left(\frac{\nu}{c^2}\right)^{\frac{1}{3}}$ is the magnetic parameter,

$$Pr = \frac{\rho v c_p}{k}$$
 the Prandtl number, $Gr = \frac{g \rho (I_w - I_{\infty})}{c}$ the

Grashof number and $Ec = \frac{(\nu c)^{\overline{3}}}{c_p(T_w - T_\infty)}$ the Eckert number.

The corresponding initial and boundary conditions for $u(\eta, \tau)$, $v(\eta, \tau)$ and $\theta(\eta, \tau)$ are

$$u=0, v=0, \theta=0 \text{ for } \eta \ge 0 \text{ and } \tau \le 0,$$

$$u=\tau, v=0, \theta=1 \text{ at } \eta=0 \text{ for } \tau >0,$$
 (16)

$$u \to 0, v \to 0, \theta \to 0 \text{ as } \eta \to \infty \text{ for } \tau >0.$$

3. NUMERICAL SOLUTION

Equations (13) - (15) are coupled, non-linear partial differential equations and these equations can not be solved exactly. However, these equations can be solved numerically. One of the most commonly used numerical methods is the finite difference technique which has better stability characteristics and is relatively simple, accurate and efficient. Another essential feature of this technique is that it is based on an iterative procedure and a tri-diagonal matrix manipulation. This method provides satisfactory results but it may fail when applied to problems in which the differential equations are very sensitive to the choice of initial conditions. In all numerical solutions the continuous partial differential equation is replaced with a discrete approximation. In this context the word *discrete* means that the numerical solution is known only at a finite number of points in the physical domain. The number of those points can be selected by the user of the numerical method. In general, increasing the number of points not only increases the resolution but also the accuracy of the numerical solution. The discrete approximation results are a set of algebraic equations that are evaluated (or solved) for the values of the discrete unknowns. The mesh is the set of locations where the discrete solution is computed. These points are called nodes and if one were to draw lines between adjacent nodes in the domain the resulting image would resemble a net or mesh.

When time dependent solutions are important, the Crank-Nicolson scheme has significant advantages. The Crank-Nicolson scheme is not significantly more difficult to implement and it has a temporal truncation error that is $O(\Delta \tau^2)$ as explained by Recktenwald [25]. The Crank-Nicolson scheme is implicit, it is also unconditionally stable [26, 27, 28]. In order to solve equations (13), (14) and (15) under the initial and boundary conditions (16), an implicit finite difference scheme of Crank-Nicolson's type has been employed. The right hand side of equations (13), (14) and (15) is approximated with the average of the central difference scheme evaluated at the current and the previous time step. The finite difference equations corresponding to equations (13), (14) and (15) are as follows

$$\frac{u_{i,j+1} - u_{i,j}}{\Delta \tau} = \frac{1}{2(\Delta \eta)^2} \Big[u_{i-1,j} - 2u_{i,j} + u_{i+1,j} + u_{i-1,j+1} - 2u_{i,j+1} + u_{i+1,j+1} \Big] + \frac{Gr}{2} \Big(\theta_{i,j+1} + \theta_{i,j} \Big) - \frac{M^2}{(1+m^2)} \Big[\Big(u_{i,j+1} + u_{i,j} \Big) - m \Big(v_{i,j+1} + v_{i,j} \Big) \Big],$$
(17)

$$\frac{v_{i,j+1} - v_{i,j}}{\Delta \tau} = \frac{1}{2(\Delta \eta)^2} \Big[v_{i-1,j} - 2v_{i,j} + v_{i+1,j} + v_{i-1,j+1} - 2v_{i,j+1} + v_{i+1,j+1} \Big] \\ - \frac{M^2}{(1+m^2)} \Big[\Big(v_{i,j+1} + v_{i,j} \Big) + m \Big(u_{i,j+1} + u_{i,j} \Big) \Big], \quad (18)$$

$$Pr\frac{\theta_{i,j+1} - \theta_{i,j}}{\Delta \tau} = \frac{1}{2(\Delta \eta)^2} \Big[\theta_{i-1,j} - 2\theta_{i,j} + \theta_{i+1,j} + \theta_{i-1,j+1} - 2\theta_{i,j+1} + \theta_{i+1,j+1} \Big] + PrEc \Bigg[\left(\frac{u_{i+1,j} - u_{i,j}}{\Delta \eta}\right)^2 + \left(\frac{v_{i+1,j} - v_{i,j}}{\Delta \eta}\right)^2 +$$

$$+M^{2}\left(u_{i,j}^{2}+v_{i,j}^{2}\right)].$$
 (19)

The initial and boundary conditions (16) become

$$u_{i,0} = 0, \ v_{i,0} = 0, \ \theta_{i,0} = 0 \text{ for all } i \neq 0,$$

$$u_{0,j} = j\Delta\tau, \ v_{0,j} = 0, \ \theta_{0,j} = 1,$$

$$u_{N,j} = 0, \ v_{N,j} = 0, \ \theta_{N,j} = 0,$$

(20)

where N corresponds to ∞ . Here the suffix *i* corresponds to η and *j* corresponds to τ . Also $\Delta \tau = \tau_{j+1} - \tau_j$ and $\Delta \eta = \eta_{i+1} - \eta_i$. Knowing the values of θ , *u* and *v* at a time τ we can evaluate the values at a time $\tau + \Delta \tau$ as follows. We substitute *i*=1,2,...,*N*-1 in the equation (19) which constitute a tri-diagonal system of equations, the system can be solved by Thomas algorithm as discussed by Carnahan et al.[29]. Thus θ is known for all values of η at time τ . Then knowing the values of θ and applying the same procedure with the boundary conditions, we calculate *u* and *v* from equations (17) and (18). This procedure is continued to obtain the solution till desired time τ . The Crank-Nicolson scheme has a truncation error of $O(\Delta \tau^2) + O(\Delta \eta^2)$, i.e. the temporal truncation error is significantly small.



Figure 2. Finite difference grids

The implicit method gives stable solutions and requires matrix inversions which we have done at step forward in time because this problem is an initial-boundary value problem with a finite number of spatial grid points, though the corresponding difference equations do not automatically guarantee the convergence of the mesh $\Delta \eta \rightarrow 0$. To achieve maximum numerical efficiency, we have used the tri-diagonal procedure to solve the two-point conditions governing the main coupled governing equations of momentum and energy. The convergence (consistency) of the process is quite satisfactory and the numerical stability of the method is guaranteed by the implicit nature of the numerical scheme. Hence, the scheme is consistent. The stability and consistency ensure convergence.

4. RESULTS AND DISCUSSION

We have presented the non-dimensional fluid velocity components u, v and the fluid temperature distribution θ for several values of the magnetic parameter M^2 , Hall parameter m, Prandtl number Pr, Grashof number Gr, Eckert number Ec and time τ against η in Figs.3-19. It is seen from Figs.3 and 4 that the primary velocity u decreases and the magnitude of the secondary velocity v increases with an increase in magnetic parameter M^2 . This indicates that the applied International Journal of Computer Applications (0975 – 8887) Volume 70– No.24, May 2013

magnetic field is effectively moving with the fluid motion. The application of the transverse magnetic field plays the role of a resistive type force (Lorentz force) on the primary flow similar to a drag force (that acts in the opposite direction of the fluid motion), which tends to resist the flow thereby reducing the primary velocity. On the other hand, the resulting Lorentzian body force will not act as a drag force but act as an aiding body force on the secondary flow. This will serve to accelerate the secondary velocity. It is observed from Figs.5 and 6 that the primary velocity u and the magnitude of the secondary velocity v increase with an increase in Hall parameter m. This is because, in general, the Hall currents reduce the resistance offered by the Lorentz force. This means that Hall currents have a tendency to increase the fluid velocity components. Figs.7 and 8 show that the primary velocity u and the magnitude of the secondary velocity v increase with an increase in Grashof number Gr. Grashof number Gr signifies the relative effect of the thermal buoyancy force to the viscous hydrodynamic force. As expected, it is observed that there is a rise in the fluid velocity due to the enhancement of thermal buoyancy force. It is due to the fact that an increase of Grashof number has a tendency to increase the thermal effect. It is observed from Figs.9 and 10 that the primary velocity u and the magnitude of the secondary velocity v decrease with an increase in Prandtl number Pr. Physically this is due to the fact that fluids with high Prandtl number have greater viscosity, which makes the fluid thick and hence move slowly. Figs.11 and 12 show that the primary velocity u and the magnitude of the secondary velocity v increase with an increase in Eckert number Ec. Figs.13 and 14 display that the primary velocity u and the magnitude of the secondary velocity v increase with an increase in time τ . Figs.15-19 show that the fluid temperature θ increases with an increase in either magnetic parameter M^2 or Hall parameter m or Grashof number Gr or Prandtl number Pr or Eckert number Ec. Eckert number is the ratio of the kinetic energy of the flow to the boundary layer enthalpy difference. The effect of viscous dissipation on the flow field is to increase the energy, yielding a greater fluid temperature and as a consequence greater buoyancy force. The increase in the buoyancy force due to an increase in the dissipation parameter enhances the temperature ditribution. It is seen from Figs.15-19 that the maximum temperature occur in the vicinity of the plate and asymptotically approaches to zero in the free stream region. This is because the effect of the magnetic parameter and Hall parameter can be felt only in the Hartmann layer and the thermal boundary layer respectively. It can be concluded that the fluid velocity and temperature raise due to viscous and Joule dissipations.



Figure 3. Primary velocity for M^2 when m=0.5, Gr=5, Ec=0.5, Pr=0.25 and $\tau=0.2$



Figure 4. Secondary velocity for M^2 when m=0.5, Gr=5, Ec=0.5, Pr=0.25 and $\tau=0.2$



Figure 5. Primary velocity for m when $M^2 = 2$, Gr = 5, Ec = 0.5, Pr = 0.25 and $\tau = 0.2$



Figure 6. Secondary velocity for m when $M^2 = 2$, Gr = 5, Ec = 0.5, Pr = 0.25 and $\tau = 0.2$



Figure 7. Primary velocity for Gr when $M^2 = 2$, m=0.5, Ec=0.5, Pr=0.25 and $\tau=0.2$



Figure 8. Secondary velocity for Gr when $M^2 = 2$, m = 0.5, Ec = 0.5, Pr = 0.25 and $\tau = 0.2$



Figure 9. Primary velocity for Pr when $M^2 = 2$, m = 0.5, Ec = 0.5, Gr = 5 and $\tau = 0.2$



Figure 10. Secondary velocity for Pr when $M^2 = 2$, m=0.5, Ec=0.5, Gr=5 and $\tau=0.2$



Figure 11. Primary velocity for Ec when $M^2 = 2$, m=0.5, Pr=0.25, Gr=5 and $\tau=0.2$



Figure 12. Secondary velocity for Ec when $M^2 = 2$, m=0.5, Pr=0.25, Gr=5 and $\tau=0.2$



Figure 13. Primary velocity for τ when $M^2 = 2$, m=0.5, Pr=0.25, Gr=5 and Ec=0.5



Figure 14. Secondary velocity for τ when $M^2 = 2$, m = 0.5, Pr = 0.25, Gr = 5 and Ec = 0.5



Figure 15. Temperature for M^2 when Pr = 0.25, m = 0.5, G = 5, Ec = 0.5 and $\tau = 0.2$



Figure 16. Temperature for *m* when Pr = 0.25, $M^2 = 2$, G=5, Ec=0.5 and $\tau=0.2$



Figure 17. Temperature for Gr when Pr = 0.25, m = 0.5, $M^2 = 2$, Ec = 0.5 and $\tau = 0.2$



Figure 18. Temperature for Pr when Gr = 5, m = 0.5, $M^2 = 2$, Ec = 0.5 and $\tau = 0.2$



Figure 19. Temperature for Ec when Pr = 0.25, m = 0.5, $M^2 = 2$, Gr = 5 and $\tau = 0.2$

Numerical values of the rate of heat transfer $-\left(\frac{\partial\theta}{\partial\eta}\right)_{\eta=0}$ at the

plate $\eta = 0$ are presented in Table 1 for several values of Eckert number Ec, Prandtl number Pr and time τ . It is seen from Table 1 that the rate of heat transfer $-\left(\frac{\partial\theta}{\partial\eta}\right)_{\eta=0}$ at the

plate $\eta = 0$ decreases with an increase in either Prandtl number Pr or time τ or Eckert number Ec. The negative values of the rate of heat transfer show that the heat is transferred from the plate to fluid.

	$\left(\partial\eta ight)_{\eta=0}$							
Pr					τ			
Ec	0.25	0.5	0.71	0.85	0.2	0.4	0.6	0.8
0.1	0.76623	0.51754	0.43898	0.28913	0.76623	0.66217	0.57816	0.56610
0.2	0.65748	0.49519	0.42438	0.27528	0.65748	0.56210	0.43391	0.35619
0.3	0.58738	0.46857	0.39607	0.23467	0.58738	0.50352	0.47549	0.32894
0.4	0.53618	0.43675	0.35442	0.16665	0.53618	0.45019	0.34108	0.20002

Table 1. Rate of heat transfer $-\left(\frac{\partial\theta}{\partial\eta}\right)_{\alpha}$ at the plate $\eta = 0$

The non-dimensional shear stresses τ_x and τ_y at the plate $\eta = 0$ due to the primary and secondary flows are respectively given by

$$\tau_x = \left(\frac{\partial u}{\partial \eta}\right)_{\eta=0}$$
 and $\tau_y = \left(\frac{\partial v}{\partial \eta}\right)_{\eta=0}$. (21)

Numerical values of the non-dimensional shear stresses τ_x and τ_y at the plate $\eta = 0$ are presented in Figs.20-24 against magnetic parameter M^2 for several values of Hall parameter m, Grashof number Gr, Prandtl number Pr, Eckert number Ec and time τ . Figs.20-23 show that the shear stress τ_x and the absolute value of the shear stress τ_y at the plate $\eta = 0$ increase with an increase in either Hall parameter m or Grashof number Gr or Prandtl number Pr or Eckert number Ec. Fig.24 shows that the shear stress τ_x at the plate $\eta = 0$ increases while the absolute value of the shear stress τ_y at the plate $\eta = 0$ decreases with an increase in time τ . On the other hand, it is observed from Figs.20-24 that the shear stress τ_x and the absolute value of the shear stress τ_y at the plate $\eta = 0$ at first increase, reach a maximum and then decrease with an increase in magnetic parameter M^2 .



Figure 20. Shear stress τ_x and τ_y for *m* when Pr = 0.25, Gr = 5, Ec = 0.5 and $\tau = 0.2$



Figure 21. Shear stress τ_x and τ_y for Gr when Pr=0.25, m=0.5, Ec=0.5 and $\tau=0.2$



Figure 22. Shear stress τ_x and τ_y for Pr when m=0.5, Gr=5, Ec=0.5 and $\tau=0.2$



Figure 23. Shear stress τ_x and τ_y for Ec when Pr = 0.25, Gr = 5, m = 0.5 and $\tau = 0.2$



Figure 24. Shear stress τ_x and τ_y for time τ when Pr = 0.25, Gr = 5, Ec = 0.5 and m = 0.5

5. CONCLUSION

Hall effects on an unsteady MHD free convective flow of a viscous incompressible electrically conducting fluid past an accelerated vertical flat plate have been studied on taking viscous and Joule dissipations into account. It is observed that the Hall currents accelerate the fluid velocity components. The fluid velocity and temperature raise due to viscous and Joule dissipations. Further, it is found that the shear stress τ_x and the

absolute value of the shear stress τ_{v} at the plate increase with

an increase in either Hall parameter or Prandlt number or Eckert number. The rate of heat transfer at the plate decreases with an increase in either Prandtl number or Eckert number or time.

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