Reliability Modeling and Profit Analysis of a Repairable System of Non-identical Units with no Operation and Repair in Abnormal Weather

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ABSTRACT

In this paper, a reliability model of a system of two nonidentical units in which one main unit (called original) is initially operative and other is a substandard unit which is kept as spare in cold standby is examined probabilistically in detail under two weather conditions - normal and abnormal. Each unit has direct complete failure from normal mode. There is a single server who visits the system immediately whenever needed. The operation and repair of the units are not allowed in abnormal weather. However, operation and repair of the units are as usual in normal weather subject to the condition that duplicate unit will not work if main unit is available for working in the system. The distributions of failure time of the units and change of weather conditions follow negative exponential while that of repair time of the units are assumed as arbitrary with different probability density functions. All the random variables are mutually independent and uncorrelated. The expressions for some important measures of system effectiveness are derived in steady state using semi- Markov process and regenerative point technique. The graphical study of MTSF, availability and profit has also been made on the basis of numerical results obtained for a particular case. The results of the present paper has also been compared with the model proposed by Malik and Deswal [6].

KEYWORDS

Repairable system, Non-identical units, Weather conditions and Stochastic analysis

1. INTRODUCTION

In view of their frequent and vital use in modern industry, the repairable systems of two or more identical units have been investigated stochastically in detail by several engineers and researchers including Gopalan and Naidu [1] and Singh [2] under strict control of environment conditions such as pollution, moisture, voltage and temperature. But in case of high cost of identical units, the non-identical unit (may be a substandard unit) might be kept as spare in cold standby not only to improve the reliability of the system but also to maintain performance of the system in emergency. Each unit is capable of performing the same kind of functions but their degree of reliability and desirability may differ from unit to

unit. Singh and Chander [3] and Chander et al. [4] discussed standby systems of non-identical units with different failure and repair policies. Also, some time it is very difficult to keep the environmental conditions under control which may fluctuate due changing climate and other natural catastrophic.

While considering this fact in mind, Malik and Barak [5] obtained reliability and economic measures of a single- unit system with no operation and repair activities in abnormal weather. Further, the cold standby systems of non-identical units under different weather conditions have not been studied so far by the researchers in the field of reliability. The application of the present work can be visualized in a system constituting of one unit as a power supply through electric transformer and other unit generator.

Hence, in the present paper, a system of two non-identical units - one is original (called main unit) and other is a substandard unit (called duplicate unit) has been analyzed probabilistically in detail under two weather conditions normal and abnormal. For this purpose a reliability model is developed. The environmental conditions when satisfied to the system correspond to normal weather; otherwise, it is supposed that the system is working under abnormal weather. Initially, the system is operative with main unit and duplicate unit is kept a spare in cold standby. Both units have direct complete failure from normal mode. Each unit is capable of performing the same set of functions with different degree of reliability and desirability. There is a single server who visits the system immediately whenever needed to do repair of the failed unit. The operation and repair of the units are not allowed in abnormal weather. However, operation and repair of the units are as usual in normal weather subject to the condition that duplicate unit will not work if main unit is available for working in the system.

The distributions of failure time of the units and change of weather conditions follow negative exponential while that of repair times of the units are taken as arbitrary. All random variables are mutually independent and uncorrelated. The switch devices and repairs are perfect. The expressions for various measures of system effectiveness such as transition probabilities, mean sojourn times, mean time to system failure (MTSF), availability, busy period of the server and profit function in steady state are derived using semi-Markov process and regenerative point technique. The numerical results giving particular values to the parameters and various costs are obtained for MTSF, availability and profit to depict their graphical behavior. The MTSF and profit of the present model have also been compared with that of the model investigated by Malik and Deswal [6].

2. NOTATIONS

E : The set of regenerative states
MO/DO : Main/Duplicate unit is good and operative
MWO /
DWO : Main/Duplicate unit is good but waiting for
operation due to abnormal weather
DCs : Duplicate unit is in cold standby mode
$\lambda / \lambda 1$: Constant failure rate of Original /Duplicate un
$\beta / \beta 1$: Constant rate of change of weather from normal
to abnormal/abnormal to normal weather
MFur/DFur : Main/duplicate unit failed and under repai
MFUR/DFUR : Main/duplicate unit failed and under
repair continuously from previous state
MFwr/DFwr : Main/duplicate unit failed and waiting fo
repair
MFWR/DFWR : Main/duplicate unit failed and waiting
for repair continuously from previous
state
MFwr /
DFwr : Main/Duplicate unit failed and waiting for
repair due to abnormal weather
MFWR /
DFWR : Main/Duplicate unit failed and waiting for
repair continuously from previous state due to
abnormal weather
g(t)/G(t) : pdf/cdf of repair time of Original unit
g1(t) / G1(t): pdf/cdf of repair time of Duplicate unit
qij (t) / Qij (t) : pdf/cdf of passage time from regenerative
state i to a regenerative state j or to a
failed state j without visiting any other
regenerative state in (0,t]
qij.kr (t) /
Qij.kr (t) : pdf/cdf of direct transition time from
Regenerative state i to a regenerative
state j or to a failed state j visiting state
k,r once in (0,t]

q ij.k,(r,s)n(t) /Qij.k,(r,s)n(t) : pd

- /Qij.k,(r,s)n(t) : pdf/cdf of direct transition time from regenerative state i to a regenerative state j or to a failed state j visiting state k once and n times states r and s.
- Mi(t) : Probability that the system is up initially in regenerative state Si at time t without visiting to any other regenerative state
- Wi(t) : Probability that the server is busy in state Si upto time t without making any transition to any other regenerative state or returning to the same via one or more non-regenerative states
- mij : The unconditional mean time taken by the system to transits from any regenerative state Si € S when time is counted from epoch of entrance into that state Sj. Mathematically, it can be written as mij=∫tQij(t)=-qij *'(0)
- : The mean sojourn time in state Si this is given by $\mu_i = E(t) = \int P(T > t) dt = \sum jmij, \text{where } T \text{ denotes the}$ time to system failure
- (S)/C/On : Symbol for Laplace Stieltjes Convolution / Laplace convolution / Laplace convolution n times
- ~/* : Symbol for Laplace Steiltjes Transform (LST)/ Laplace Transform (LT)
- '(desh) : Used to represent derivative

The following are the possible transition states of the system

 $S_0 = (MO, DCs), S_1 = (MFur, DO), S_2 = (\overline{MWO}, \overline{DCs}),$

 $S_3 = (\overline{MFwr}, \overline{DWO}),$

S₄ =(MFUR,DFwr),S₅=(MO,DFur),

 $S_6=(\overline{MFwr}, \overline{DFWR}), S_7=(MFur, DFWR),$

 $S_8 = (\overline{MWO}, \overline{DFwr}), S_9 = (MFwr, DFUR)$

 $S_{10} = (MFWR, DFwr), S_{11} = (MFWR, DFur)$

The states S_0 , S_1 , S_2 , S_3 , S_5 , S_8 are regenerative while the states S_4 , S_6 , S_7 , S_9 , S_{10} , S_{11} are non -regenerative as shown in figure 1.

State Transition Diagram



- □ Failed-State
- Regenerative point

Fig. 1

3. **RELIABILITY INDICES**

3.1 Transition Probabilities and Mean **Sojourn Times**

Simple probabilistic considerations yield the following expressions for the non-zero elements

$$p_{ij}=Q_{ij}(\infty)=\int q_{ij}(t)dt$$
 as

$$p_{01} = \frac{\lambda}{\beta + \lambda}, p_{02} = \frac{\beta}{\beta + \lambda}, p_{10} = g^{*}(\beta + \lambda_{1}),$$

$$p_{13} = \frac{\beta}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}), p_{14} = \frac{\lambda_{1}}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1}),$$

 $p_{20}=1, p_{31}=1, p_{45}=g^{*}(\beta), p_{46}=1-g^{*}(\beta), p_{50}=g_{1}^{*}(\beta+\lambda),$

$$p_{58} = \frac{\beta}{\beta + \lambda} (1 - g_1 * (\beta + \lambda)), p_{59} = \frac{\lambda}{\beta + \lambda} (1 - g_1 * (\beta + \lambda)),$$

$$p_{67} = 1, p_{75} = g^*(\beta), p_{76} = 1 - g^*(\beta), p_{85} = 1, p_{91} = g_1 * (\beta),$$

$$p_{9,10} = 1 - g_1 * (\beta), p_{10,11} = 1, p_{11,1} = g_1 * (\beta), p_{11,10} = 1 - g_1 * (\beta)$$
(1)
It can be easily verified that
$$p_{01} + p_{02} = p_{10} + p_{13} + p_{14} = p_{20} = p_{31} = p_{45} + p_{46} = p_{50} + p_{58} + p_{59} = 1,$$

$$p_{67} = p_{75} + p_{76} = p_{85} = p_{91} + p_{9,10} = p_{10,11} = p_{11,1} + p_{11,10} = 1$$

(2) The mean sojourn times (μ_i) in the state S_i are

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$$\begin{split} \mu_{0} &= \frac{1}{\beta + \lambda}, \ \mu_{1} &= \frac{1}{\beta + \lambda_{1}} (1 - g^{*}(\beta + \lambda_{1})), \mu_{2} \\ &= \frac{1}{\beta_{1}}, \mu_{3} = \frac{1}{\beta_{1}}, \mu_{4} = \frac{1}{\beta} (1 - g^{*}(\beta)) \\ &, \mu_{5} = \frac{1}{\beta + \lambda} (1 - g_{1}^{*}(\beta + \lambda)), \\ \mu_{6} &= \frac{1}{\beta_{1}}, \mu_{7} = \frac{1}{\beta} (1 - g^{*}(\beta)), \mu_{8} = \frac{1}{\beta_{1}}, \\ \mu_{9} &= \frac{1}{\beta} (1 - g_{1}^{*}(\beta)), \mu_{10} = \frac{1}{\beta_{1}}, \mu_{11} = \frac{1}{\beta} (1 - g_{1}^{*}(\beta)) \end{split}$$

(3)

it can be observed that

$$\begin{split} m_{01} + m_{02} &= \mu_0 \;, m_{10} + m_{13} + m_{14} = \mu_1 \;, m_{20} = \mu_2, m_{31} = \mu_3, \\ m_{45} + m_{46} &= \mu_4, \; m_{50} + m_{58} + m_{59} = \mu_5, \\ m_{67} &= \mu_6, m_{75} + m_{76} = \mu_7, m_{85} = \mu_8, m_{91} + m_{9,10} = \mu_9, m_{10,11} = \mu_{10}, m_{11,10} = \mu_{11} \end{split}$$

 $\begin{array}{l} \mu_{1}^{'} = m_{10} + m_{13} + m_{15.4} + m_{15.4,(6,7)}^{n}, \mu_{5}^{'} = m_{50} + m_{51.9} + m_{51.9,(10,11)}^{n} \\ + m_{58} \end{array}$

3.2 Reliability and Mean Time to System Failure (MTSF)

Let $\phi_i(t)$ be the cdf of first passage time from

regenerative state i to a failed state.

Regarding failed state as absorbing state, we have

following recursive relations for $\phi_{i}(t)$:

$$\phi_0(t) = Q_{01}(t) \otimes \phi_1(t) + Q_{02}(t) \otimes \phi_2(t)$$

$$\phi_{1}(t) = Q_{10}(t) \otimes \phi_{0}(t) + Q_{13}(t) \otimes \phi_{1}(t) + Q_{14}(t)$$

$$\phi_{2}(t) = Q_{20}(t) \otimes \phi_{0}(t), \quad \phi_{3}(t) = Q_{31}(t) \otimes \Phi \phi_{1}(t)$$

(6)

Taking LST of above relation (6) and solving for $\widetilde{\phi}_0(s)$ We have

$$\mathbf{R}^*(s) = \frac{1 - \widetilde{\phi}_0(s)}{s}$$

(7)

The reliability of the system model can be obtained by taking Laplace inverse transform of (7).

The mean time to system failure (MTSF) is given by

$$\text{MTSF} = \lim_{s \to o} \frac{1 - \widetilde{\phi}_0(s)}{s} = \frac{N_1}{D_1}$$

where

$$\begin{split} N_1 = & p_{01}(p_{13}\mu_3 + \mu_1) + (1 - p_{13})(\mu_0 + p_{02}\mu_2) \\ D_1 = & p_{01}p_{14} \end{split}$$

3.3 Steady State Availability

Let $A_i(t)$ be the probability that the system is in up-state at instant 't' given that the system entered regenerative state i at t = 0. The recursive

(8)

relations for $A_i(t)$ are given as

$$A_0(t) = M_0(t) + q_{01}(t) \odot A_1(t) + q_{02}(t) \odot A_2(t)$$

 $A_1(t) = M_1(t) + q_{10}(t) \odot A_0(t) + q_{13}(t) \odot A_3(t)$

+ $(q_{15.4}(t)+q_{15.4,(6,7)}^{n}(t))$ ©A₅(t)

 $A_2(t) = q_{20}(t) \odot A_0(t) , A_3(t) = q_{31}(t) \odot A_1(t)$

 $A_5(t)=$

$$\begin{split} &M_5(t) + q_{50}(t) @A_0(t) + (q_{51.9}(t) + q_{51.9,(10,11)}{}^n(t)) @A_1(t) + q_{58}(t) \\ & @A_8(t) \end{split}$$

$$A_8(t) = q_{85}(t) \odot A_5(t)$$

(10)

where $M_i(t)$ is the probability that the system is up initially in state $Si \in E$ is up at time t without visiting to any other regenerative state, we have

$$M_0(t) = e^{-(\beta+\lambda)t}$$
, $M_1(t) = e^{-(\beta+\lambda_1)t} \overline{G(t)}$, $M_5(t) = e^{-(\beta+\lambda_1)t}$

$$(11) \qquad (11)$$

Taking LT of above relations (10) and solving for

 $A_0^*(s)$. The steady state availability is

given by

$$A_0(\infty) = \lim_{s \to 0} s A_0^*(s) = \frac{N_2}{D_2}$$
(12)

where

 $N_2 = \mu_0((1-p_{13})(1-p_{58})-p_{14}p_{59}) + \mu_1 p_{01}(1-p_{58}) + p_{01}p_{14}\mu_5$ and

D₂=(1-

 $p_{58})(p_{01}(\mu'_1+p_{13}\mu_3)+m_{01}p_{10})+p_{14}(p_{01}(\mu'_5+p_{58}\mu_8)+m_{01}p_{50})+(m_{02}+p_{02}\mu_2)((1-p_{58})(1-p_{13})-p_{14}p_{59})$

(13)

3.4 Busy period analysis for server

Let $B_i(t)$ be the probability that the server is busy in repairing the unit at an instant

't' given that the system entered regenerative state i at t=0.The recursive relations for $B_i(t)$ are as follows:

$$B_0(t) = q_{01}(t) \odot B_1(t) + q_{02}(t) \odot B_2(t)$$

 $B_1(t) = W_1(t) + q_{10}(t) @B_0(t) + q_{13}(t) @B_3(t) + (q_{15.4}(t) \\$

 $+q_{15.4,(6,7)}^{n}(t)) @B_{5}(t)$

 $B_2(t)=q_{20}(t) @B_0(t), B_3(t)=q_{31}(t) @B_1(t)$

 $B_{5}(t) = W_{5}(t) + q_{50}(t) \otimes B_{0}(t) + (q_{51.9}(t) + q_{51.9,(10,11)}^{n}(t))$

 $OB_1(t)+q_{58}(t)OB_8(t)$

 $B_8(t) = q_{85}(t) \odot B_5(t) \tag{13}$

where $W_i(t)$ be the probability that the server is busy in state S_i due to failure upto time t without making any transition to any other regenerative state or returning to the same via one or more non-regenerative states.

so,

$$\begin{split} W_{1}(t) = e^{-(\beta+\lambda_{1})t} \overline{G(t)} &+ (\lambda_{1}e^{-(\beta+\lambda_{1})t} \mathbb{C}1) \overline{G(t)} , W_{5}(t) = e^{-(\beta+\lambda_{1})t} \overline{G_{1}(t)} &+ (\lambda e^{-(\beta+\lambda)t} \mathbb{C}1) \overline{G_{1}(t)} & (14) \end{split}$$

Taking LT of above relations (13) . And, solving for B_0^* (s), the time for which server is busy due to repair is given by

$$B_0^*(\infty) = \lim_{s \to 0} s B_0^*(s) = \frac{N_3}{D_2}$$

where

$$N_3 = p_{01}(W_1^*(0)(1-p_{58})+p_{14}W_5^*(0))$$

and D_2 is already mentioned.

3.5 Expected number of visits by the server

Let $N_i(t)$ be the expected number of visits by the server in (0,t] given that the system entered

the regenerative state i at t=0. The recursive relations for $N_i(t)$ are given as : $N_0(t) = Q_{01}(t) \ (1+N_1(t)) + Q_{02}(t) \ (N_2(t))$

$$N_1(t) = Q_{10}(t) \widehat{S} N_0(t) + Q_{13}(t)$$

 $SN_3(t)+(Q_{15,4}(t)+Q_{15,4,(6,7)}^n(t))SN_5(t)$

 $N_2(t)=Q_{20}(t) \otimes N_0(t)$, $N_3(t)=Q_{31}(t) \otimes N_1(t)$

$$\begin{split} N_5(t) = & Q_{50}(t) (SN_0(t) + (Q_{51.9}(t) + Q_{51.9,(10,11)}^n(t)) (SN_5(t) + Q_{58} \\ (t) (SN_8(t)) \end{split}$$

$$N_8(t) = Q_{85}(t) \otimes N_5(t)$$
 (15)

Taking LST of relations (15) and solving for $N_0^{0}(s)$

The expected number of visits per unit time by the server is given by

$$N_0(\infty) = \lim_{s \to 0} s N_0^{0}(s) = \frac{N_4}{D_2}$$

where

 $N_4 = p_{01}((1-p_{13})(1-p_{58})-p_{14}p_{59})$ and D_2 is already specified.

3.6 Profit Analysis

The profit incurred to the system model in steady state can be obtained as

 $P_i = K_0 A_0 - K_1 B_0 - K_2 N_0$

where

K₀=Revenue per unit up-time of the system

K₁=Cost per unit for which server is busy

 K_2 = Cost per unit visit by the server and A_0, B_0, N_0 are already defined.

4. CONCLUSION

Giving some particular values to the parameters and various costs, the numerical results for MTSF, availability and profit function are obtained to depict their graphical behavior with respect to normal weather rate (β_1) keeping fixed values of other parameters as shown in figures 2, 3 and 4 respectively. From figure 2, it is observed that MTSF declines with the increase of normal weather rate (β_1) and failure rates (λ , λ_1) of the units. But MTSF increases with increase of abnormal weather rate (β) and repair rate (α) of the main unit. Figures 3 and 4 show that availability and profit of the system model go on increasing with increase of normal weather rate (β_1) and repair rates (α and α_1) of the units. However, there is a downward trend in the values of these measures as and when values of abnormal weather rate (β) and failure rates (λ and λ_1) increase. On the basis of the results obtained for a particular case, it is concluded that a cold standby system of non-identical units will be more profitable if it is allowed to operate under controlled weather i.e. normal weather. If we compare the MTSF and Profit of the present model with that of the model Malik and Deswal [2012], it is found that MTSF of both the models is same however, the present model is less profitable. Hence, we conclude that priority to the operation

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and repair of original unit should be given over the duplicate unit in order to improve the profit of the model.

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6. REFERENCES

- Gopalan, M.N and Naidu, R.S (1982): Stochastic Behavior of a Two -Unit Repairable System subject to Inspection. Microelectron. Reliab., Vol. 22, pp. 717-722.
- [2] Singh, S.K (1989): Profit evaluation of Two -Unit Cold Standby System with Random Appearance and Disappearance Time of the Service Facility. Microelectron. Reliab., Vol. 29, pp. 705-709.

- [3] Singh, Mukender and Chander, S. (2005): Stochastic Analysis of Reliability Models of an Electric Transformer and Generator with Priority and Replacement. Journal of Decision and Mathematical Sciences, Vol. 10 (1-3), pp. 79-100.
- [4] Chander, S.; Singh, Mukender and Kumari, Meena (2007): Cost Benefit Analysis of a Stochastic Analysis of an Electric Transformer and Generator. Journal of Pure and Applied Mathematika Sciences, Vol. LXVI, No. 1-2, pp. 13-25.
- [5] Malik, S.C. and Barak, M.S (2009): Reliability and Economic Analysis of a System Operating under Different Weather Conditions. Journal of Proc. Mat. Acad. Sci, India, Sect. A, Vol. 79, pt. II, pp205-213.
- [6] Malik, S.C. and Deswal, Savita (2012): Stochastic Analysis of a Repairable System of Non-Identical Units with Priority for Operation and Repair Subject to Weather Conditions. International Journal of Computer Applications, Vol. 49(14),pp.33-41.









Fig.4