

Fig 2: Return loss versus frequency plot.

The radiation pattern in 2D is shown in Fig 3. The radiation is obtained between -90 degree to +90 degree which represents that it is above the ground plane.

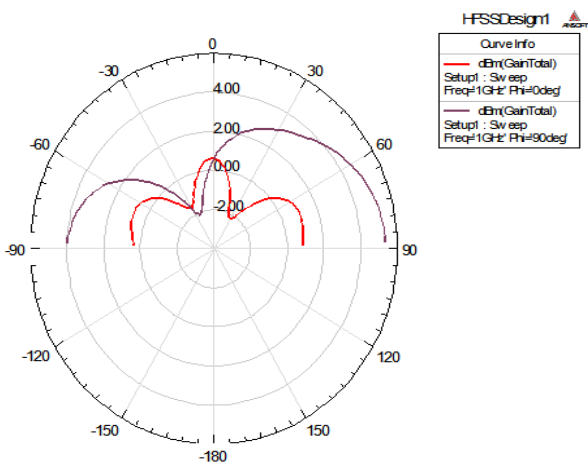


Fig 3: Radiation pattern in 2D.

The radiation pattern in 3D is presented in Fig 4.



Fig 4: Radiation pattern in 3D.

Simulated VSWR of proposed antenna v/s frequency plot is presented in Fig 5.

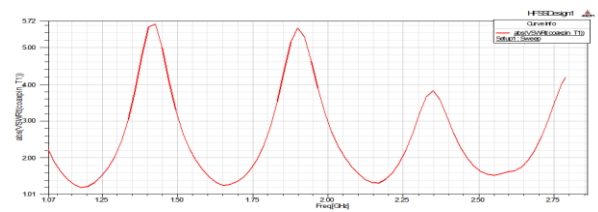


Fig 5: VSWR v/s frequency plot.

It may be observed that VSWR of proposed antenna is minimum at four frequencies 1.17GHz, 1.65 GHz, 2.12 GHz and 2.50 GHz.

The axial ratio variation with frequency of simulated proposed antenna is shown in Fig 6.

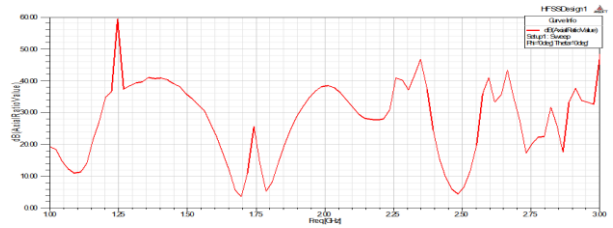


Fig 6: axial ratio v/s frequency plot.

From the axial ratio v/s frequency plot, it may be observed that value of axial ratio for proposed arrangement is greater than desired 3dB value means it is linearly polarized.

Smith chart represents the variation of simulated input impedance of proposed arrangement as a function of frequency which is shown in Fig 7.

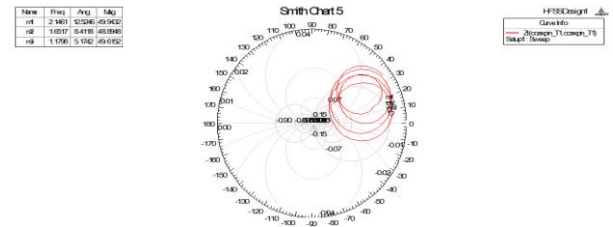


Fig 7: Smith Chart of proposed antenna

The input impedance of this proposed arrangement at resonance frequency 1.1798 GHz 1.65 GHz and 2.14 GHz is 49.6152j[5.1742, 48.8948j[8.4118 and 49.9432j[12.5246 which again suggests excellent matching between feed arrangement and antenna at resonant frequency.

Gain of proposed antenna using HFSS is presented in Fig 8. Gain value at resonant frequency 2.12 GHz is 18dBm.

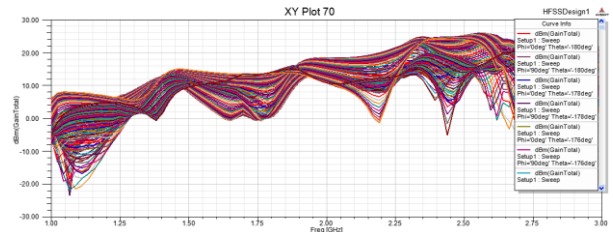


Fig 8: Gain v/s frequency plot

4. PERFORMANCE ANALYSIS OF BOWTIE ANTENNA ARRAY

It is observed from the simulation results that antenna has small bandwidth of 16.23% at 1.17GHz frequency. For further enhancement of bandwidth, two strategies are adopted.

4.1 Variation in Ground Plane Length

It is observed that bandwidth of antenna is improved by changing the length of ground plane and there is very less variation in bandwidth when the width of ground plane is varied represented in Fig 9 and Table 1.

Table 1. Effect of ground plane length

S. No.	Ground plane length(y) in mm	% Bandwidth		
		Fr=1.17 GHz	Fr=1.65 GHz	Fr=2.12 GHz
1	20	16.23	12.72	8.37
2	50	17.09	12.12	8.83
3	100	15.38	12.05	8.37
4	150	16.23	12.12	8.37

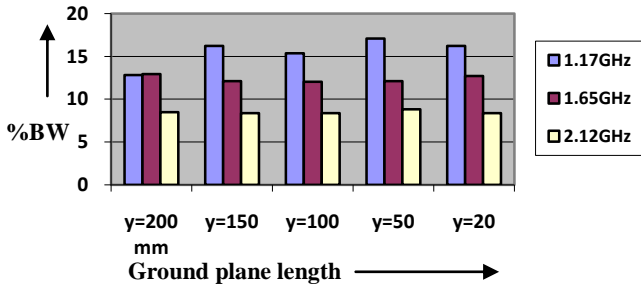


Fig 9: Bandwidth versus ground plane length plot.

As the length y of ground plane is decreased the bandwidth is increased. Optimum ground plane length is 50 mm where bandwidth is 17.09% at 1.17GHz and 8.83% at 2.12GHz frequency.

4.2 Variation in Substrate Materials

As refractive index of substrate material is decreased, the bandwidth of antenna is increased but losses are also increased. Three materials are used: FR4 ($\epsilon_r=4.4$), Epoxy Kevlar ($\epsilon_r=3.6$) and Rogers RT/Duroid ($\epsilon_r=2.2$). Comparative analysis of bandwidth is represented in Fig 10 and Table 2.

Table 2. Effect of substrate material on bandwidth

S. No.	Substrate Material	% Bandwidth			
		First resonant frequency	Second resonant frequency	Third resonant frequency	Forth resonant frequency
1	FR4	17.09	12.12	8.83	--
2	Epoxy Kevlar	17.82	12.707	12.765	8.77
3	Roggers RT/Duroid	40.95	18.4	14.66	17.97

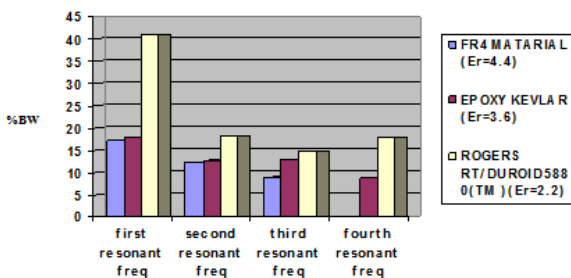


Fig 10: Bandwidth plot for different substrate material

It may be observed from Fig 10 that there is significant enhancement in bandwidth for substrate of low dielectric constant. Maximum bandwidth is achieved by using RT/Duroid substrate but losses are also increased but if these losses are under permissible limit for some applications than it is good option.

The effect of refractive index on return loss is represented in Fig 11 and Table 3.

Table 3. Effect of substrate material on return loss

S. No	Substrate Material	Return loss in dB			
		First resonant freq.	Second resonant freq.	Third resonant freq.	Forth resonant freq.
1	FR4	-21	-19	-17	-13.5
2	Epoxy Kevlar	-40	-30	-24.5	-15.5
3	Roggers RT/Duroid	-25	-24	-41	-29

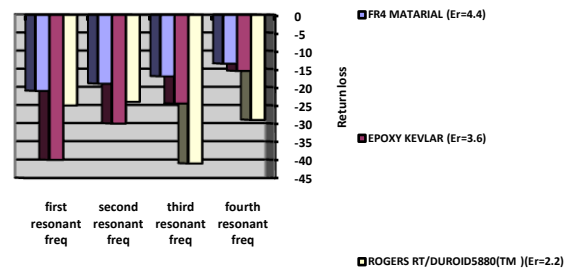


Fig 11: Return loss for different materials

It may be observed from the Fig 11 and Table 3 that return loss is increased at first and second resonant frequencies for Rogers RT/Duroid substrate which has lowest dielectric constant in above mentioned geometries. The wide bandwidth factor can be utilized if losses are acceptable for any specific application.

5. CONCLUSION

In this paper, the performance of Bow tie antenna array is analyzed. Bandwidth is increased due to decreasing the ground plane length and almost constant due to changing the ground plane width. As the refractive index is decreased the bandwidth of proposed antenna is increased. For Rogers RT/Duroid material, the same geometry provides 40.95%, 18.40%, 14.66%, 17.97% and 8.85% at 1.05GHz, 1.63GHz, 2.25GHz, 2.92GHz and 3.5GHz respectively which can be used for WCDMA, Mobile Satellite services, point to point, TV pickup and subscriber radio system (SRS). Stacked arrangement of patches and modified ground plane structure can be used for achieving more enhancements in bandwidth. Gain can be further enhanced by increasing the no. of elements in array configuration.

6. REFERENCES

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