

3. OPERATION PRINCIPLE

The operation of the proposed topology is divided into four different circuit stages in each switching cycle. Each stage shown in Fig. 5 will be explained in details as follows.

3.1.1 Modes of Operation

A. Mode I ($P_{pv} > P_{ac}$)

This mode occurs whenever the generated PV power is greater than the output ac power. The switching period T_s is divided into four intervals.

Stage 1

During this stage, as seen in Fig. 5(a), switch S1 is turned ON. Then, the magnetizing current in transformer ramps up from zero to i_{L1} -peak1.

Stage 2

This stage starts when the main switch S1 is turned OFF, while the switches in the secondary side are still OFF, at this instant, the magnetizing current starts charging the decoupling capacitor CD through D1 and D3.

Stage 3

During this stage, the current i_2 is released through one of the secondary windings and the corresponding ac switch, either S3 or S4, The grid voltage during one switching period u_{ac} can be assumed to be constant; as the current i_2 reach to zero.

Stage 4

As the current i_2 decreases to zero, this stage starts where all the switches are turned OFF. The capacitor C_r and inductor L_r keep pumping energy to the grid, while the flux in the flyback transformer is reset.

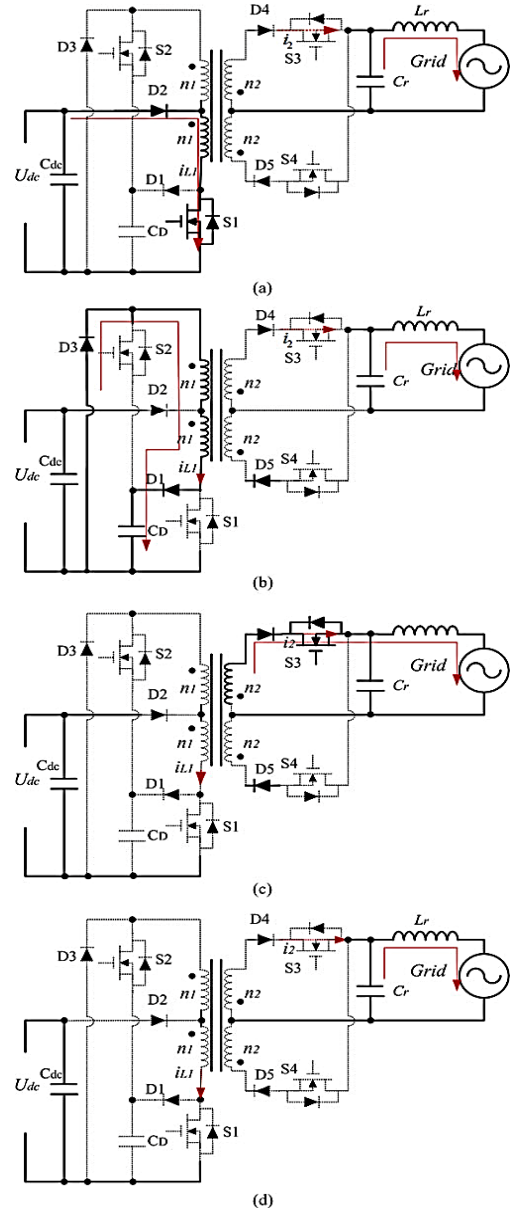


Fig 3: Detailed circuit operation stages during mode-I.(a)Stage1[t_0-t_1],(b)Stage2[t_1-t_2],(c) Stage3 [t_2-t_3], and(d) Stage4[t_3-t_4]

B. Mode II ($P_{pv} < P_{ac}$)

Stage 1

This stage is quite similar to stage 1 in mode I. S1 is turned ON, and the magnetizing inductance stores energy from PV panel through D1, T1, and S1, The magnetizing current ramps up linearly until it reaches i_{L1} -peak.

To maintain constant power from PV panel, the peak current in this stage should be fixed as the input voltage from PV panel is assumed to be constant in the steady state.

Stage 2

This mode starts when the magnetizing current reaches i_{L1} -peak. At that instant S2 is turned ON, and all the diodes at the primary side are reversed biased,. As the magnetizing current in one primary winding is coupled into another primary winding during this stage, the

magnetizing current $i_{L\text{-peak21}}$ will be halved. The energy stored in the decoupling capacitor C_D continues charging the new inductor with two windings in series.

The new magnetizing current ramps up linearly until it reaches $i_{L\text{-peak22}}$, where the energy stored in the magnetizing inductance equals the required energy to be pumped into the ac side on the average basis of one switching period.

Stage 3

Once S_1 and S_2 are turned OFF simultaneously at t_3 , the current at secondary side $i_2(t)$ is released through one of the secondary side. Since the voltage ripple across the capacitor C_r during one switching period is negligible.

Stage 4

This stage is the same as stage 4 in mode I. No current flows through transformer windings, and the transformer is in magnetizing reset state. The output current is maintained by C_r and grid-tied inductor L_r .

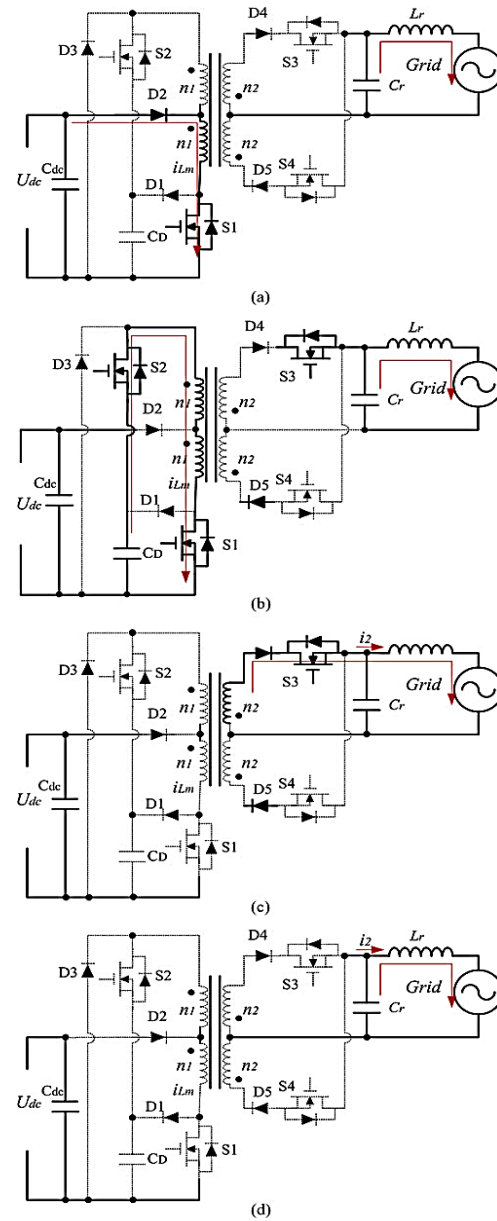
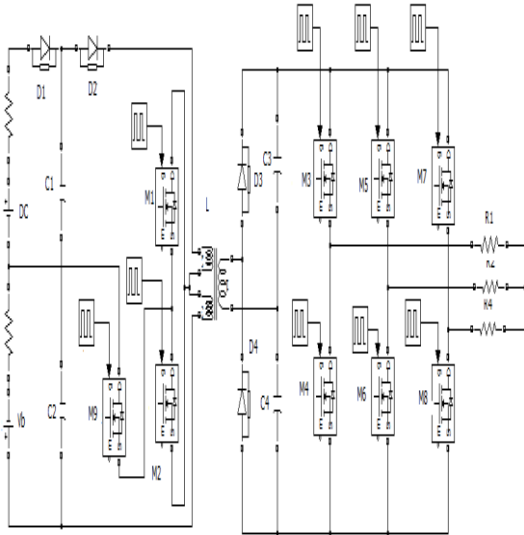


Fig 4: Detailed circuit operation stages during mode II. (a)Stage 1[$t_0 - t_1$], (b) Stage 2[$t_1 - t_2$], (c) Stage 3[$t_2 - t_3$], and (d) Stage 4[$t_3 - t_4$].

4. PROPOSED SYSTEM

The proposed system is the three port flyback micro inverter like conventional system but the output of the proposed system is three phase. This system contains battery instead of decoupling capacitor which presented in the conventional system.

The transformer is isolated transformer which has higher efficiency with less loss. This battery backup provides the supply to the transformer when the input system fails.



5: Proposed Technology

4.1.1 Mode of Operations

A. Normal Mode

The input supply V_{dc} is supplying the load by turning on the switches $M1$, $M9$, and the diodes $D1$ and $D2$ are conducting. On the secondary capacitor $C4$ and diode $D3$ is conducting and the switches $M3$, $M6$ and $M7$ are turned on connecting the load for the three phase mode.

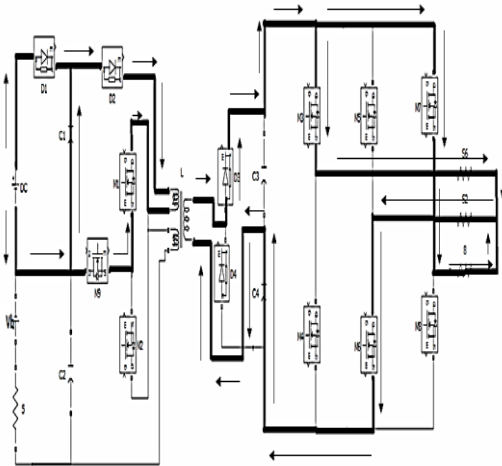


Fig 6: Normal operation of proposed circuit

B. Battery Charging Mode

The input V_{dc} is supplying the load through the diodes $D1$, $D2$, $D3$ and the switches $M3$, $M6$ and $M7$ are turned on by connecting the load.

Fig

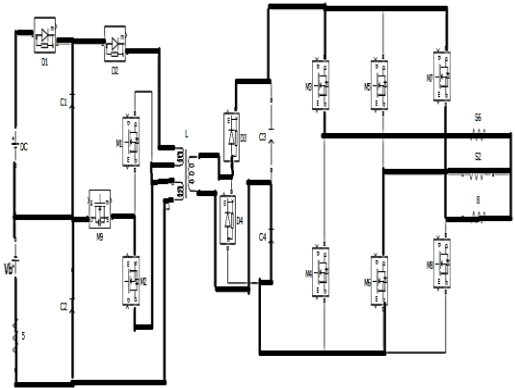


Fig 7: Battery charging mode

The battery (V_b) is charged by turning on the switches $M9$ and $M2$

C. Battery Supplying Mode

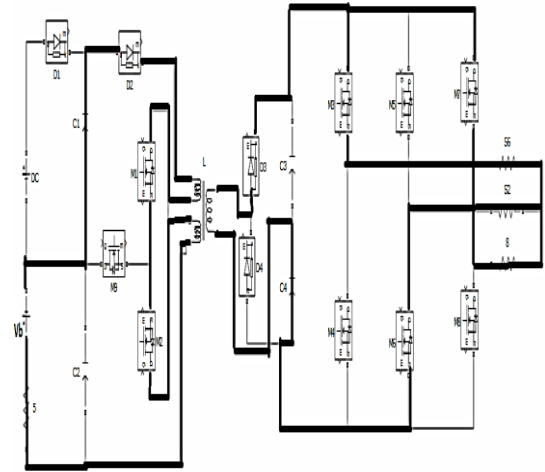


Fig 8: Battery supplying mode

The battery voltage V_b is supplying the load through the diode $D2$, capacitor $C1$, $C4$ and diode $D3$ and the switches $M1$, $M2$, $M3$, $M6$, and $M7$ are turned on.

5. Experimental Results

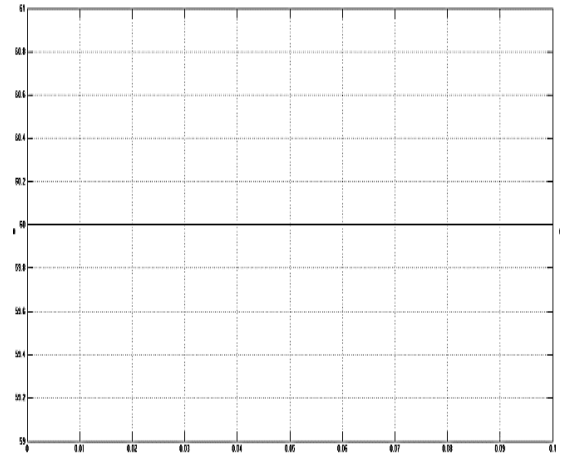


Fig 9: Input waveform of the conventional model

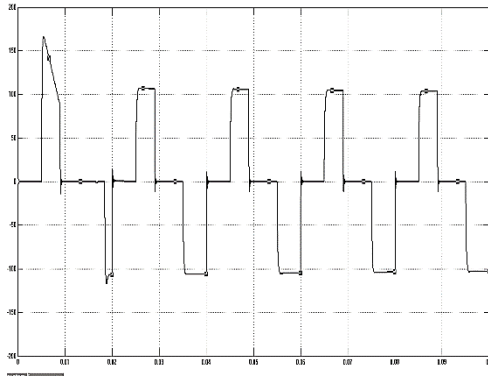


Fig 10: Output waveform of the conventional system (Normal Mode)

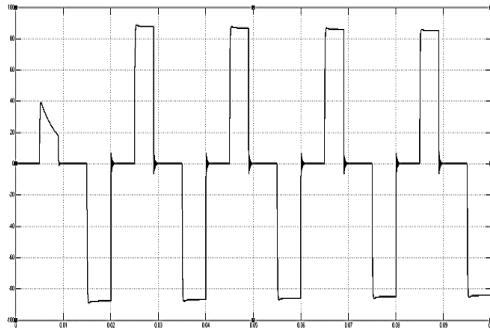


Fig 11: Output waveform of the conventional system (Backup Mode)

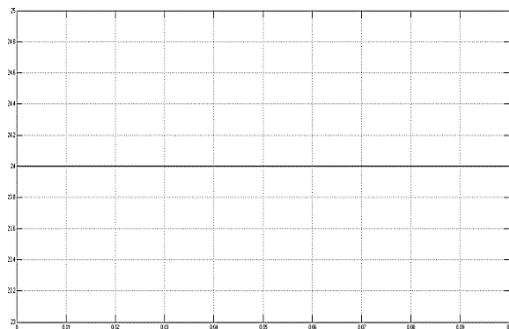


Fig 12: Input waveform of the proposed model

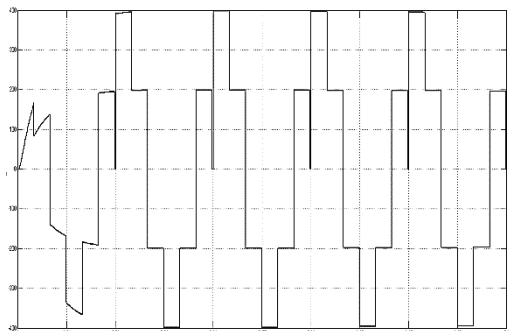


Fig 13: Three phase output wave form of the proposed model.

6. CONCLUSION

A new microinverter topology is proposed. It primarily aims for the ac-module PV systems. The proposed topology employs a new battery backup technique and it is easily

replacable if the battery failure. Hence, it will have a long life span comparable to the PV Panel. The Isolated high frequency transformer is used in this model so there is no leakage current in the primary side of the transformer. So the efficiency will be high and the final output of the proposed model is three phase output.

7. REFERENCES

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