# Computing Solution of the Flow due to a Nozzle

Bounab Noura
Laboratory of Pure and Applied
Mathematics LPAM
Department of Mathematics.
University of M'sila Algeria

Bouderah Brahim
Laboratory of Pure and Applied
Mathematics LPAM
Department of Computer Science.
University of M'sila Algeria

#### **ABSTRACT**

The present work consider a bidimensional flow with a free surface of an incompressible and inviscid fluid due to a curved nozzle, where the effect of surface tension is not neglected. The computed accurate numerical solution with surface tension  $T \neq 0$  via a serie truncation. However, there is a solution for each value of the Weber number  $\alpha > 5$ 

**Keywords**: Computation, Free surface, nozzle, Weber number

#### 1. INTRODUCTION

Free surface flows have been studied by many authors F.Dias & aL[1] B. Bouderah & aL [2] [4] [9],, H. Mekias & al [3] [5],. Analytical data for flows issuing from horizontal nozzle far upstream are rather common literature, Gurevich [6]. Most of this results come from earlier work by Von Mises [7], F. Toison [8].

#### 2. NUMERICAL RESOLUTION

#### 2.1 Problem Statement and Solution Method

Let us consider a steady two-dimensional flow of an incompressible, irrotational and inviscid fluid issuing from a curved nozzle which forms an angle  $\beta=\frac{\pi}{4}$  with the horizontal (see figure 1).

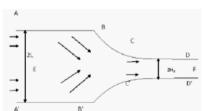


Fig:1 The Z- plan.

One takes because of symmetry of the flow field ,we need only consider the upper half of the flow region witch is between the x-axis and the streamline *ABCD* (Figure.2).

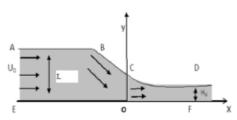


Fig 2: The upper half of the flow region Z-plan

We note that the flow is uniform and the velocity is equal to U, and L as the unit length. We introduce the complex velocity potential  $f = \varphi + i\psi$  without loss of generality, we choose  $\psi = 0$  on the streamline ABCD,  $\varphi = 0$ , at(x,y) = (0,1) and  $\psi = -1$  on EOF. In order to use the conformal mapping techniques; the upper half of the flow region in the Z- plane will be mapped via the potential function f onto the semi-infinite strip  $\{-\infty < \varphi < +\infty, -1 < \psi < 0\}$  (see Figure 3).

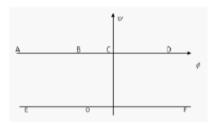


Fig 3 : The f- Plan

We map it into the fourth quarter unit disk of the auxiliary  $\omega$ -plan by the transformation. (see Figure 5)

$$f = \frac{2}{\pi} \ln \left( \frac{2i\omega}{1 + \omega^2} \right) \tag{1}$$

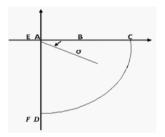


Fig 4: The w-Plan

On the free surface the pressure is constant and then the Bernoulli equation becomes

$$q^2 - \frac{2}{\alpha} \left( \frac{1}{R} \right) = 1 \quad , \quad on CD$$
 (2)

Where q is the flow speed, R the radius of curvature of the free surface. The complex velocity rewrite in new variables  $\tau$  and  $\theta$  as  $\xi = u - iv = exp(\tau - i\theta)$ . In dimensionless variables and using  $\tau$  and  $\theta$ , (2) becomes

$$exp(2\tau) + \frac{\pi}{\alpha} \tan(\sigma) \frac{\partial \theta}{\partial \varphi} = 1$$
 , on CD (3)

Where  $\alpha$  is the Weber number and  $\omega = |\omega| exp(i\sigma)$  ,  $-\frac{\pi}{2} < \sigma < 0$ 

Since  $\xi$  must have singularity at two points correspond respectively at the point  $\omega_{C}$ ,  $\omega_{B}$  in the  $\omega$  – plan , local behaviors of :

$$\omega_B = b$$
,  $\omega_C = 1$  Are:

at 
$$\omega_B = b$$
:  $\xi \sim c_1(b^2 - \omega^2)^{\frac{1}{2}}$  as  $\omega \to b$ 

with: 
$$c_1 = \left(\frac{3}{4}\right)^{\frac{1}{2}} \alpha(k_1)^{\frac{1}{2}}$$

at 
$$\omega_C = 1$$
:  $\xi \sim c_2 (1 - \omega^2)^{2 - \frac{2\gamma}{\pi}}$  as  $\omega \to 1$ 

with: 
$$c_2 = \left(\frac{\pi}{4}\right)^{1-\frac{\gamma}{\pi}} \alpha(k_2)^{-1-\frac{\gamma}{\pi}}$$

Following [1], [2] we seek  $\xi(\omega)$  in the form:

$$\xi(\omega) = (b^2 - \omega^2)^{\frac{1}{2}} (1 - \omega^2)^{2 - \frac{2\gamma}{\pi}} exp\left(\sum_{k=1}^{\infty} a_k \omega^{2(k-1)}\right)$$
 (4)

The coefficients  $a_k$  are to be found. The free surface CD is mapped by the transformation (1) into the fourth quarter unit circle. And we use the notation

$$\omega = |\omega| exp(i\sigma)$$
 ,  $-\frac{\pi}{2} < \sigma < 0$ 

In the relation (4), we obtain:

$$exp(\tau(\sigma)) = (2\cos\sigma)^{2-\frac{2}{\pi}}exp(\sum_{k=1}^{\infty}a_k\cos(2(k-1)\sigma))$$

$$\theta(\sigma) = -\left(3\sigma - \frac{2\gamma}{\pi}\sigma + \sum_{k=1}^{\infty} a_k \sin(2(k-1)\sigma)\right)$$

#### 2.2 Computational Method

Following Vanden-Broeck, Mekias and Bouderah ([1]- [4]), we solve the problem by truncating the infinite series in (4) after N terms. The N coefficients  $a_n$  are found by collocation.

# 2.2.1 Computation of the coefficients $(a_k)_{k=1,n}$ of the series(4)

The initial data  $A^{(0)}$ ,  $\varepsilon$ ; kmax.

## **1.** Computing: $A = (a_i)_{i=1,n}$

$$E_{ij}^{(K)} = \frac{\partial f_i(A)}{\partial a_j} \bigg|_{A=A^{(K)}} \} j = 1, \dots, n$$

$$f_i^{(K)} = 1 + (2\cos\sigma_i)^{2-\frac{2}{\pi}} exp\left(\sum_{k=1}^{\infty} a_k \cos(2(k-1)\sigma_i)\right)$$

$$+ \frac{\pi}{\alpha} \tan(\sigma_i) *$$

$$* \left[ -\left(3\sigma_i - \frac{2\gamma}{\pi}\sigma_i + \sum_{k=1}^{\infty} a_k \sin(2(k-1)\sigma_i)\right) \right]_{\varphi_{\sigma_i}}$$

$$i = 1, \dots, n$$

#### 2. Solve the linear system:

$$\sum_{k=1}^{n} E_{ij}^{(K)} \Delta A_{j}^{(k)} = f_{i}^{(k)} ] i = 1, ..., n$$

#### 3. Computing:

$$A_i^{(k+1)} = A_i^{(k)} + \Delta A_i^{(k)} i = 1, 2, ..., n$$

#### 4. If:

$$|f_i(A^{(k+1)})| < \in ]i = 1,2,...,n$$
  
 $k > kmax$   
is verified

#### 5. Stop

**Remark**: using the algorithm of Jordan with total pivotation implied.

Some coefficients  $(a_k)$  of the series (4) for different values of number of weber Alpha

Table 1. Alpha=10 <sup>+8</sup>				
n	an	n	an	
1	4.9540 10 <sup>-9</sup>	26	-3.4598 10 <sup>-12</sup>	
2	-3.3038 10 <sup>-9</sup>	27	-3.1448 10 <sup>-12</sup>	
3	-6.5878 10 <sup>-10</sup>	28	-2.8749 10 <sup>-12</sup>	
4	-2.8280 10 <sup>-10</sup>	29	-2.6205 10 <sup>-12</sup>	
5	-1.5660 10 <sup>-10</sup>	30	-2.4008 10 <sup>-12</sup>	
6	-9.9716 10 <sup>-11</sup>	31	-2.1913 10 <sup>-12</sup>	
7	-6.8764 10 <sup>-11</sup>	32	-2.0088 10 <sup>-12</sup>	
8	-5.0419 10 <sup>-11</sup>	33	-1.8333 10 <sup>-12</sup>	
9	-3.8378 10 <sup>-11</sup>	34	-1.6789 10 <sup>-12</sup>	
10	-3.0269 10 <sup>-11</sup>	35	-1.5291 10 <sup>-12</sup>	
11	-2.4371 10 <sup>-11</sup>	36	-1.3960 10 <sup>-12</sup>	
12	-2.0097 10 <sup>-11</sup>	37	-1.2659 10 <sup>-12</sup>	
13	-1.6776 10 <sup>-11</sup>	38	-1.1489 10 <sup>-12</sup>	
14	-1.4253 10 <sup>-11</sup>	39	-1.0337 10 <sup>-12</sup>	
15	-1.2198 10 <sup>-11</sup>	40	-9.2850 10 <sup>-13</sup>	
16	-1.0585 10 <sup>-11</sup>	41	-8.2386 10 <sup>-13</sup>	
17	17 -9.2252 10 <sup>-12</sup>		-7.2610 10 <sup>-13</sup>	
18	18 -8.1316 10 <sup>-12</sup>		-6.2697 10 <sup>-13</sup>	
19	-7.1834 10 <sup>-12</sup>	44	-5.2987 10 <sup>-13</sup>	
20	-6.4072 10 <sup>-12</sup>	45	-4.2478 10 <sup>-13</sup>	
21	-5.7190 10 <sup>-12</sup>	46	-3.0426 10 <sup>-13</sup>	
22	-5.1473 10 <sup>-12</sup>	47	-1.2774 10 <sup>-13</sup>	
23	-4.6308 10 <sup>-12</sup>	48	2.7122 10 <sup>-13</sup>	
24	-4.1967 10 <sup>-12</sup>	49	2.8671 10 <sup>-12</sup>	
25	-3.7981 10 <sup>-12</sup>	50	-9.2445 10 <sup>-11</sup>	

Table 2. Alpha=100				
n	a <sub>n</sub>	n	an	
1	4.9540 10 <sup>-3</sup>	26	-3.3669 10 <sup>-6</sup>	
2	-3.3038 10 <sup>-3</sup>	27	-3.0633 10 <sup>-6</sup>	
3	-3.5878 10 <sup>-4</sup>	28	-2.7964 10 <sup>-6</sup>	
4	-2.7944 10 <sup>-4</sup>	29	-2.5580 10 <sup>-6</sup>	
5	-1.5469 10 <sup>-4</sup>	30	-2.3479 10 <sup>-6</sup>	
6	-9.8100 10 <sup>-5</sup>	31	-2.1304 10 <sup>-6</sup>	
7	-6.7683 10 <sup>-5</sup>	32	-1.9939 10 <sup>-6</sup>	
8	-4.9462 10 <sup>-5</sup>	33	-1.7119 10 <sup>-6</sup>	
9	-3.7681 10 <sup>-5</sup>	34	-1.7470 10 <sup>-6</sup>	
10	-2.9628 10 <sup>-5</sup>	35	-1.3771 10 <sup>-6</sup>	
11	-2.3885 10 <sup>-5</sup>	36	-1.4867 10 <sup>-6</sup>	
12	-1.9645 10 <sup>-5</sup>	37	-1.1970 10 <sup>-6</sup>	
13	-1.6409 10 <sup>-5</sup>	38	-1.0499 10 <sup>-6</sup>	
14	-1.3905 10 <sup>-5</sup>	39	-1.1413 10 <sup>-6</sup>	
15	-1.1934 10 <sup>-5</sup>	40	-9.0073 10 <sup>-7</sup>	
16	-1.0309 10 <sup>-5</sup>	41	-7.2244 10 <sup>-7</sup>	
17	-9.0182 10 <sup>-6</sup>	42	-7.9707 10 <sup>-7</sup>	
18	-7.9273 10 <sup>-6</sup>	43	-6.9981 10 <sup>-7</sup>	
19	-7.0043 10 <sup>-6</sup>	44	-4.7084 10 <sup>-7</sup>	
20	-6.2445 10 <sup>-6</sup>	45	-4.3504 10 <sup>-7</sup>	
21	-5.5700 10 <sup>-6</sup>	46	-4.7365 10 <sup>-7</sup>	
22	-5.0134 10 <sup>-6</sup>	47	-3.4155 10 <sup>-7</sup>	
23	-4.5150 10 <sup>-6</sup>	48	-1.5623 10 <sup>-7</sup>	
24	-4.0908 10 <sup>-6</sup>	49	-1.2595 10 <sup>-7</sup>	
25	-3.7062 10 <sup>-6</sup>	50	-8.2648 10 <sup>-6</sup>	

#### 2.2.2 Calculate of the free surface

On the interval  $\left[\frac{-\pi}{2}, 0\right]$ , we introduce (N+1) on mesh points,

$$\sigma_I = \frac{\pi}{2(N+1)} \left( I - \frac{1}{2} \right), \qquad I = 1, \dots, N+1$$

We obtain (N+1) nonlinear algebraic equations of (N+1) unknowns  $a_k$ , the shape of the free surface is determined by integrating numerically the relation:

$$\frac{\partial x}{\partial \sigma} = \frac{2}{\pi} \cot \sigma_I \left( 2 \cos \sigma_I \right)^{2 - \frac{2\gamma}{\pi}} exp \left( \sum_{k=1}^N a_k \cos(2(k-1)\sigma_I) \right)$$

$$\times \cos \left( 3\sigma - \frac{2\gamma}{\pi} \sigma_I \right)$$

$$+ \sum_{k=1}^N a_k \sin(2(k-1)\sigma_I)$$

$$\frac{\partial y}{\partial \sigma} = \frac{2}{\pi} \cot \sigma_I \left( 2 \cos \sigma_I \right)^{2 - \frac{2\gamma}{\pi}} exp \left( \sum_{k=1}^N a_k \cos(2(k-1)\sigma_I) \right)$$

$$\times \sin \left( 3\sigma - \frac{2\gamma}{\pi} \sigma_I \right)$$

$$+ \sum_{k=1}^N a_k \sin(2(k-1)\sigma_I)$$

The Euler's method was sufficient to solve numerically the relation above.

# 3. DISCUSSION AND REPRESENTATION OF RESULTS

### 3.1 Solution without Surface Tension

$$(\alpha \rightarrow \infty , g = 0)$$

When the effect of surface tension is neglected in the free surface condition [9], the number of Weber  $\alpha \to \infty$ , the equation (4) becomes :

$$exp(2\tau) = v_x^2 + v_y^2 = 1$$
 , on the free surface

Where the forces of gravity are not taken account; the exact and analytical solution is find via free stream line theory of Kirchhoff. Also, a numerical solutions were computed using the procedure described above for  $\beta = \left(\frac{\pi}{4}\right)$ , the solution is wrote like:  $\xi(\omega) = \omega$ , it's the same obtained by Khrichoff (Batchelor 1967).

In this case, the numerical computational shows that there is a critical value  $\alpha_{max}=1000$ ,  $\alpha>\alpha_{max}$ , when  $\alpha>\alpha_{max}$ , within the  $\varepsilon\approx 10^{-8}$  error. We show in this case that the free surface flow for the Weber number  $\alpha=10^{+8}$  and the exact solution find analytically are the same. (see figure 5).

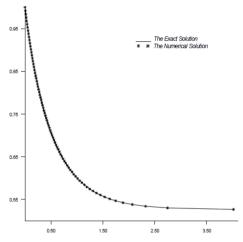


Fig 5. The exact and numerical solutions

### 3.2 Surface Tension Effect $T \neq 0$ , g = 0

When the surface tension is included in the free surface conditions, the numerical procedure shows that there exists a solution for various  $\alpha \geq \alpha^* = 5$  for the angle  $\beta = \frac{\pi}{4}$ . As n increase the coefficients  $a_n$  decrease rapidly, it is also noted that the series

$$\sum_{k=1}^{+\infty} a_k t^{2k}$$

Is absolutely convergent because we have:

$$\sum_{k=1}^{+\infty} \left| a_k t^{2k} \right| \le \sum_{k=1}^{+\infty} \left| a_k \right| \le \sum_{k=1}^{+\infty} \left( \frac{5}{6} \right)^k.$$

(see figure 6-10).

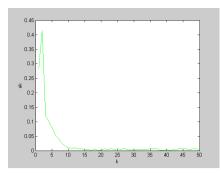


Fig 6: The coefficients  $|a_k|$  for  $\alpha = 5.5$ 

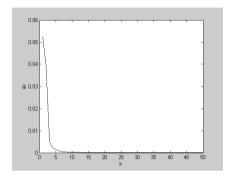


Fig 7: The coefficients  $|a_k|$  for  $\alpha = 10$ 

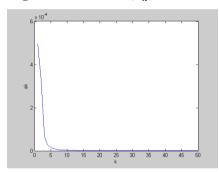


Fig 8: The coefficients  $|a_k|$  for  $\alpha = 10^3$ 

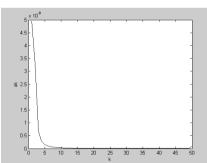


Fig 9: The coefficients  $|a_k|$  for  $\alpha = 10^8$ 

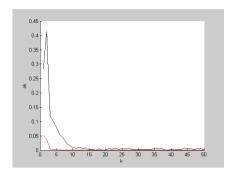


Fig 10: Comparison between the coefficients  $|a_k|$  for  $\alpha = 10$  and  $\alpha = 5.5$ 

The numerical scheme ceases to converge for all the values of the parameter  $\alpha \leq \alpha^*$ . It is noted that the convergence is faster when  $\alpha \rightarrow \infty$  and it is slower when  $\alpha \rightarrow \alpha^* = 5$ . Finally, the form of the free surface is represented for various values of the Weber number  $\alpha$  (See Figure.11.)

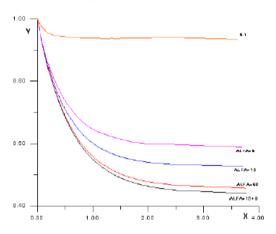


Fig 11 : The free surface flow for various values of the Weber number  $\alpha$ 

#### 4. CONCLUSION

In a forthcoming work, and after some research studies in this domain, we raise the interesting other work problem by adopting the method of the finite volume technique, to find the approach solution.

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